



Palestra:

“Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes”

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# Modelagem Computacional como uma Ferramenta para o Monitoramento de Estruturas de Pontes Existentes

Túlio Nogueira Bittencourt

Grupo de Modelagem de Estruturas de Concreto – GMEC

Escola Politécnica da Universidade de São Paulo

São Paulo - Brazil



Túlio N. Bittencourt  
*Universidade de São Paulo*  
*São Paulo - Brazil*



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## Organization

- Needs for advanced research in the field of assessment of bridges in Brazil
- Reasons for the safety assessment of existing bridges
- Modeling methodologies for global/local analysis of bridges
- Bridge simulation for fatigue analysis
- Methodologies of Dynamic Analysis of Bridges for High Speed Trains
- Conclusions



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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# Needs for advanced research in the field of assessment of bridges in Brazil



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Universidade de São Paulo  
São Paulo - Brazil



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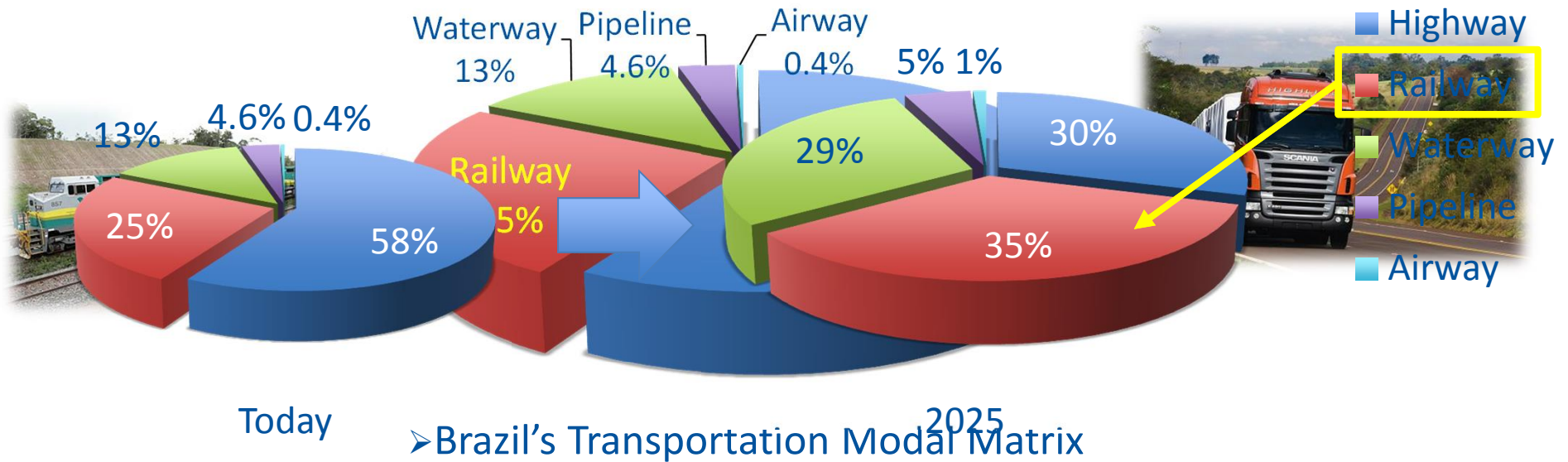
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# Needs for advanced research in the field of assessment of bridges in Brazil

➤ The Brazilian Plan for Logistics and Transportation suggests that the Transportation Mode Matrix should evolve as below





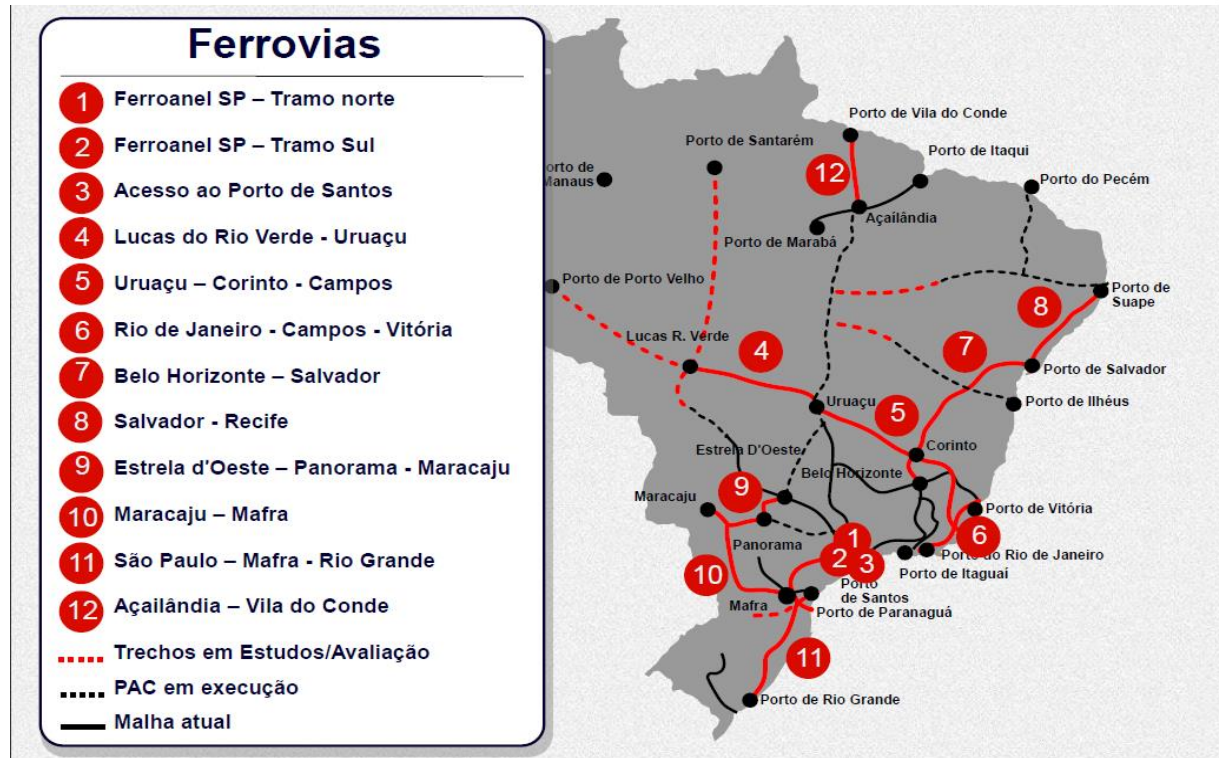


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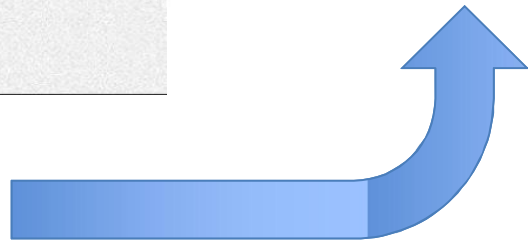
# Needs for advanced research in the field of assessment of bridges in Brazil



Future



Existing



This scenario poses some new challenges to the railway infrastructure in Brazil.



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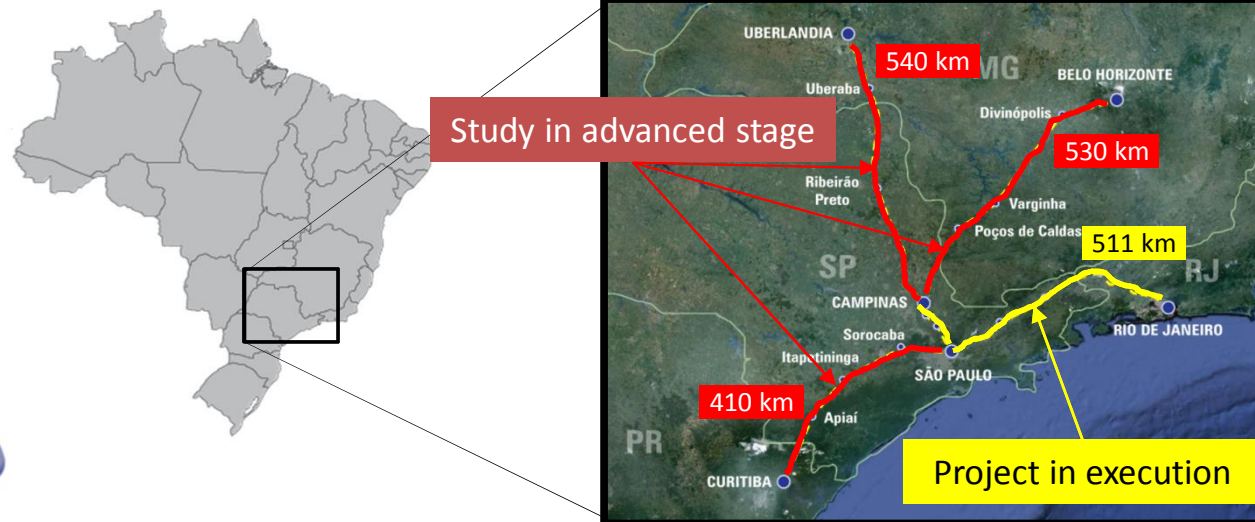
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## Needs for advanced research in the field of assessment of bridges in Brazil

### ➤ High Speed Rail Project



▪ The high speed tracks are supposed to link the major Brazilian cities in the southeast portion of the country.

▪ In total the Brazilian High Speed network will be 3,100 km long and it is supposed to be completed in the next 20 or 25 years.



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# Reasons for the safety assessment of existing bridges



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Universidade de São Paulo  
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## Reasons for the safety assessment of existing bridges

- ✓ Exceptional heavy loads and new traffic load requirements;
- ✓ Changes such as deterioration, mechanical damage, repair or change of use;
- ✓ Bridge designed according to outdated design code;
- ✓ Concern when the maximum permit load is going to be increased;



**Is the bridge still sufficiently safe???**

**Need for Advanced Analysis Tools**

Source: SB4.2, (2007). “Guideline for Load and Resistance Assessment of Existing European Railway Bridges: Advices on the use of advanced methods”. Prepared by Sustainable Bridges- a project within EU FP6.



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Universidade de São Paulo  
São Paulo - Brazil



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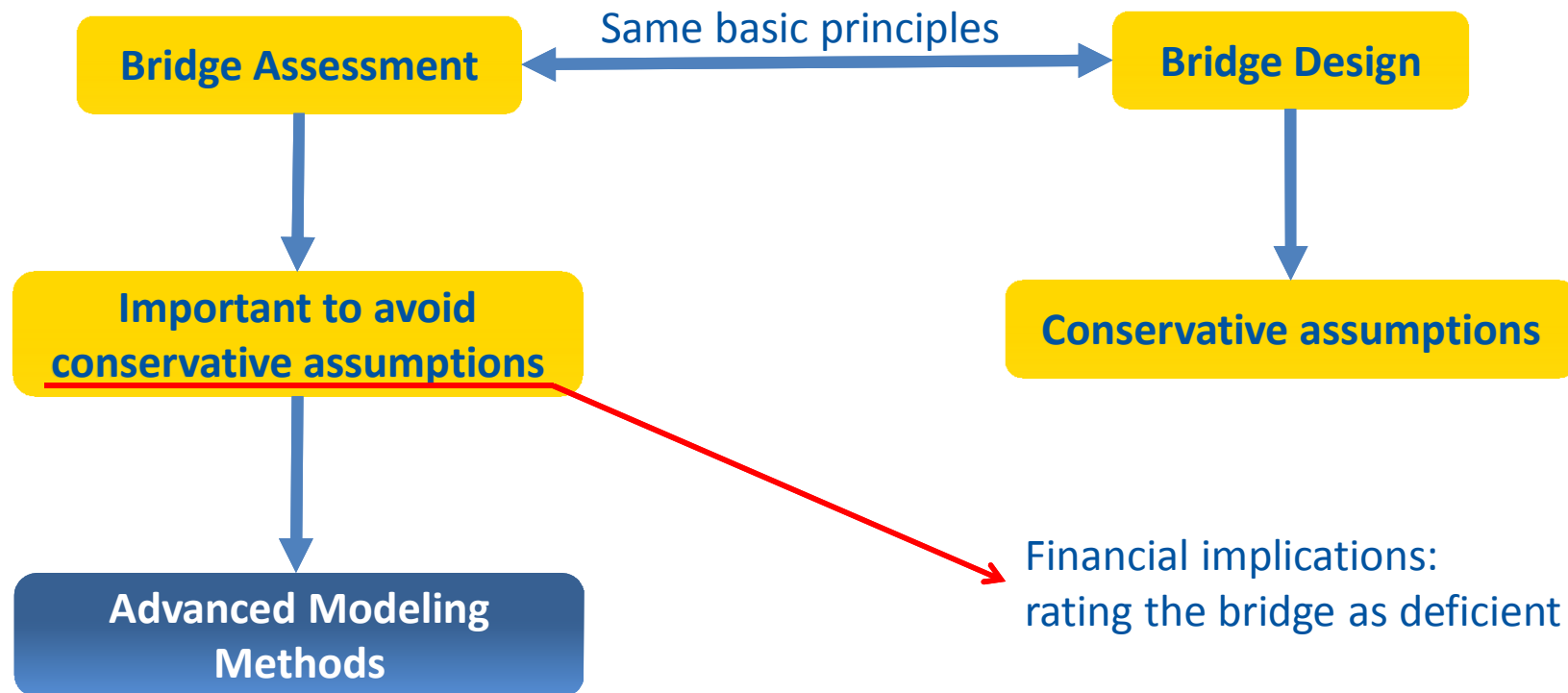


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## Reasons for the safety assessment of existing bridges







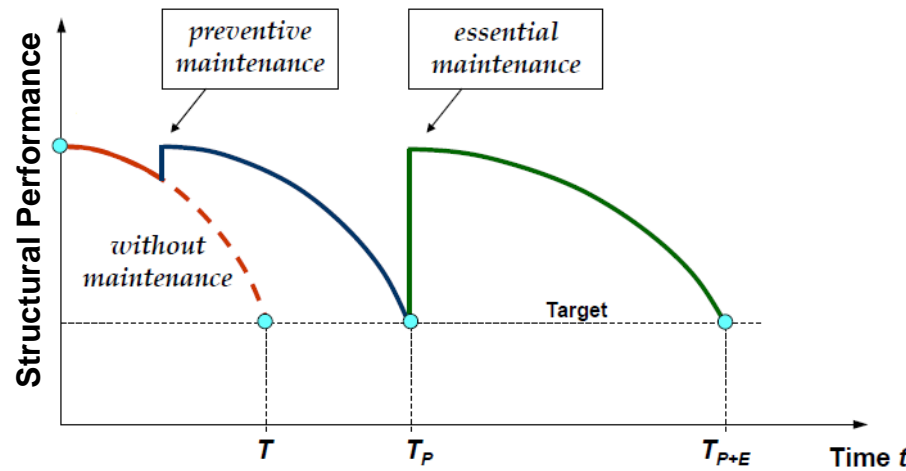
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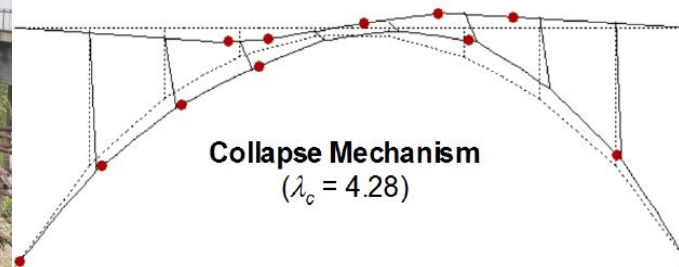
## Reasons for the safety assessment of existing bridges

asses



s:

- Linear x Non-linear;
- Dynamic with/without vehicle-bridge interaction;
- Better load models;
- Better resistance parameters;
- Incorporation of the results from monitoring;
- Damage modeling: fatigue, corrosion...
- Collapse mechanisms;



Courtesy: Prof. Fábio Biondini- Politecnico di Milano



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Universidade de São Paulo  
São Paulo - Brazil



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# Modeling methodologies for global/local analysis of bridges



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Universidade de São Paulo  
São Paulo - Brazil



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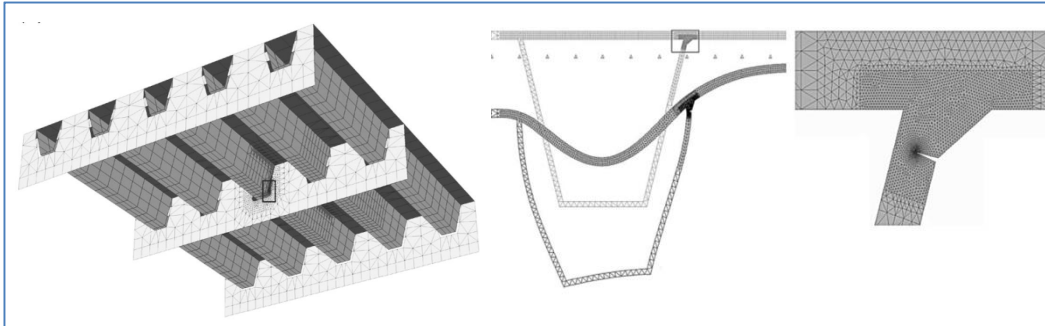
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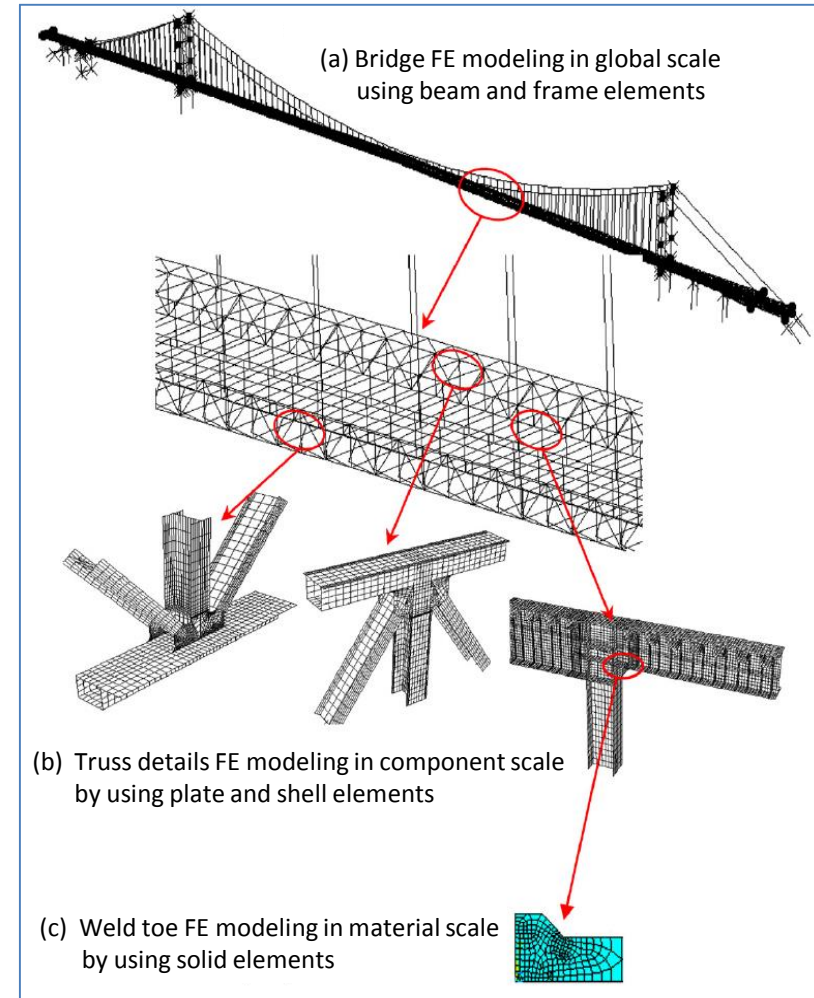
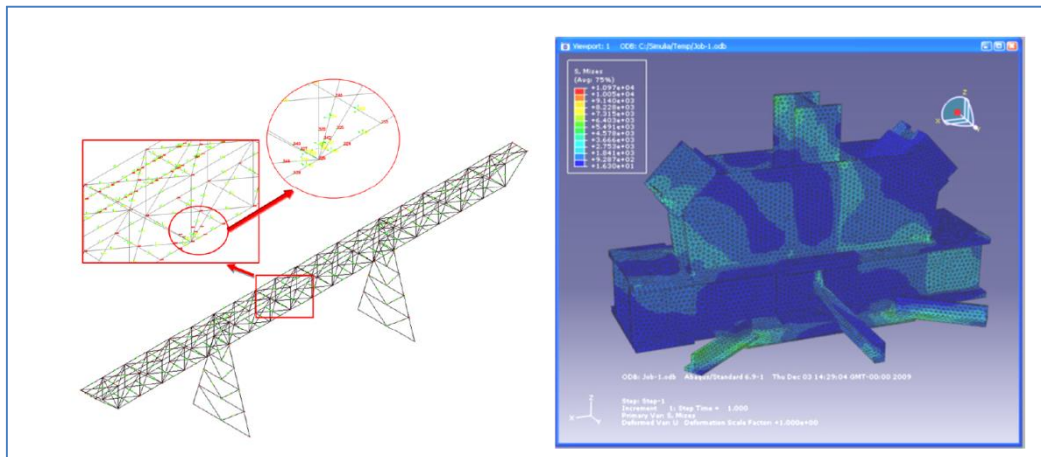


## Global and local analysis

KISS and DUNAI (2002)



LEITE et al. (2010)



LI et al. (2007)





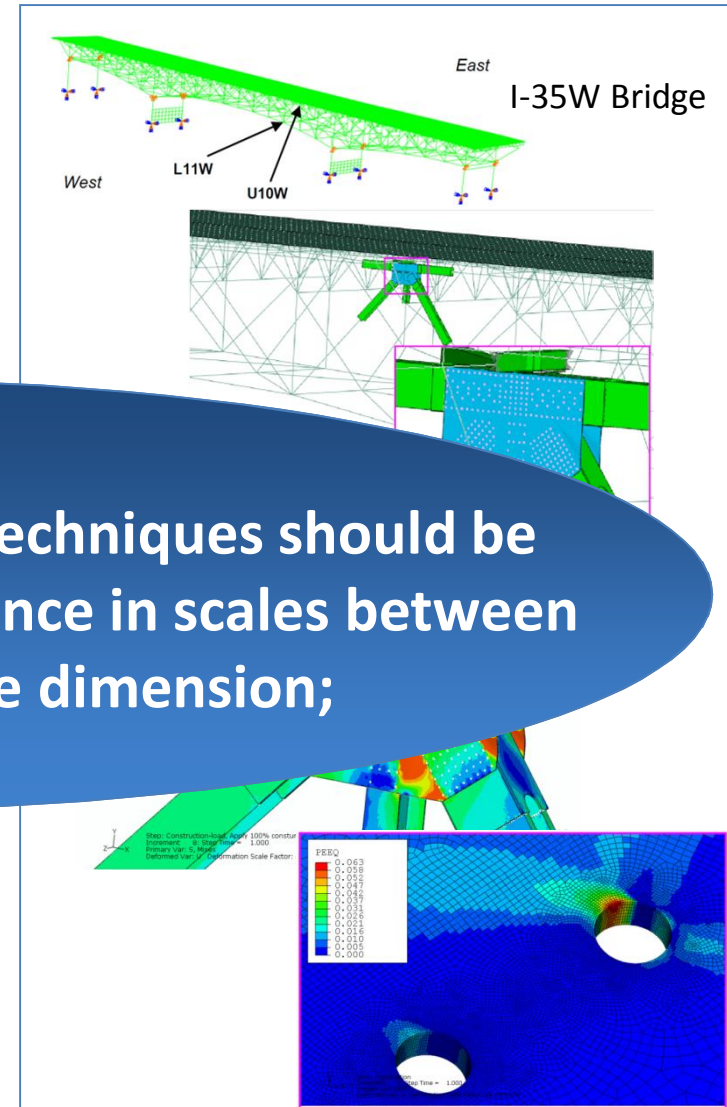
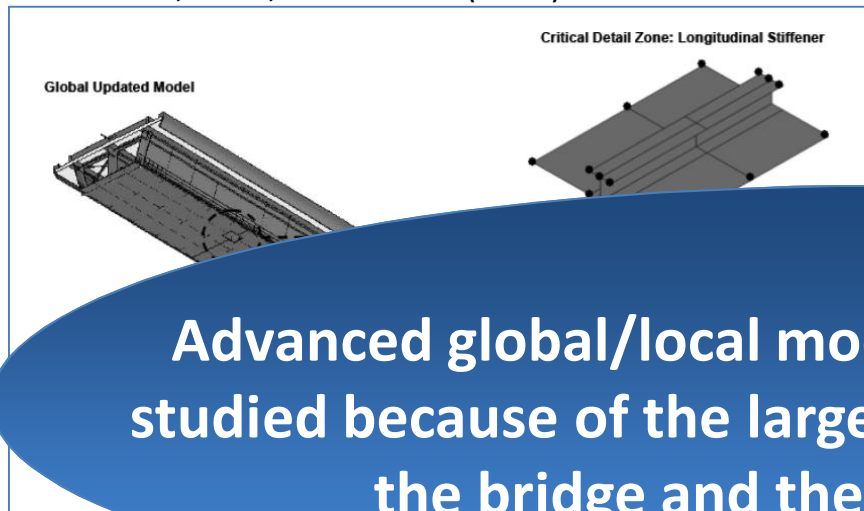
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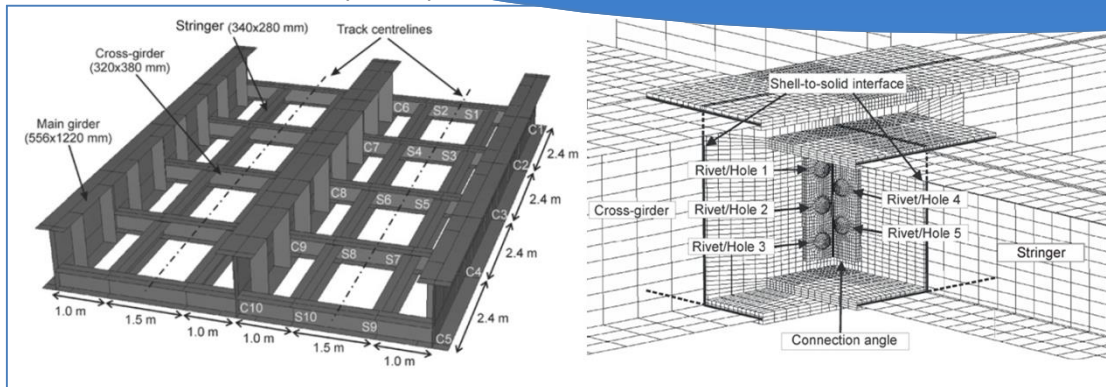
## Global and local analysis

CHELLINI; LIPPI; SALVATORE (2012)



Advanced global/local modeling techniques should be studied because of the large difference in scales between the bridge and the damage dimension;

IMAM; RIGHINIOTIS (2010)



NATIONAL TRANSPORTATION SAFETY BOARD (2008)



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## A modeling methodology for global/local analysis

Comments:

- ABAQUS FEA software has been used because it supports programming and I/O commands;
- This approach can be automated: the tasks are programmed and performed automatically without interaction of the user while the program is executed;
- The methodology has been developed to enable the coupling between the FEA software and customized user subroutines, based on Python scripting and MatLab programming;
- The loop parameterization-simulation-parameterization is time-consuming and requires multiple calls of the physical model;



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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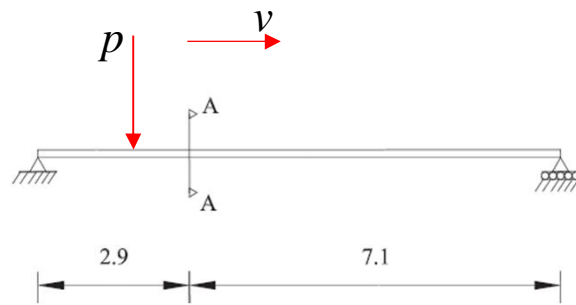


## A modeling methodology for global/local analysis

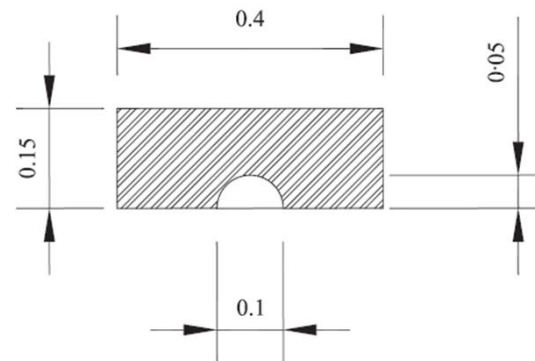
➤ Application: fatigue crack growth analysis of bridges

Fracture Mechanics: extraction of Dynamic Stress Intensity Factors

➤ Example studied by ALBUQUERQUE; DE CASTRO; CALÇADA (2012)



(a) Beam dimension and crack location [m]



(b) Crack dimensions (section A-A) [m]

$$E = 210 \text{ GPa}$$

$$\nu = 0.3$$

$$\rho = 7850 \text{ kg / m}^3$$

$$p = 100 \text{ kN}$$

$$v = 250 \text{ m / s (900 km / h)}$$





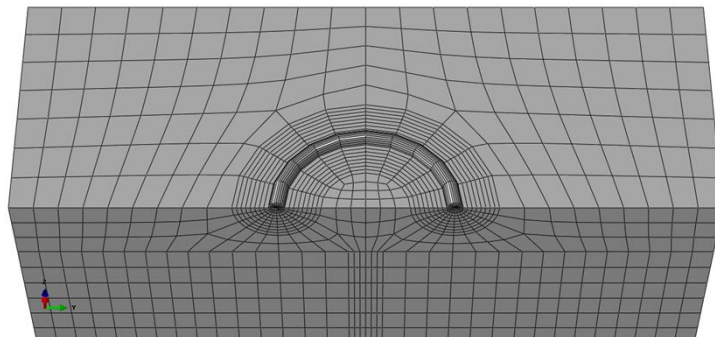
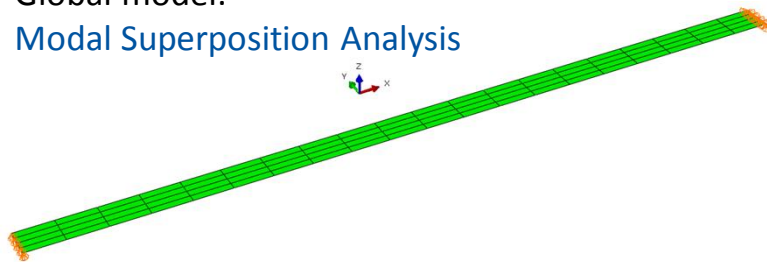
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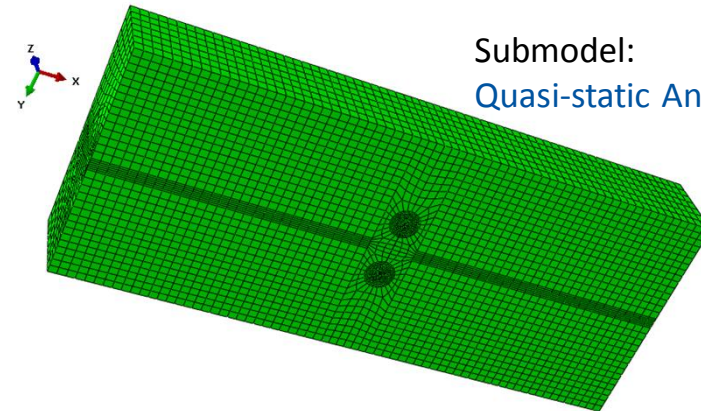
Fracture Mechanics: extraction of  
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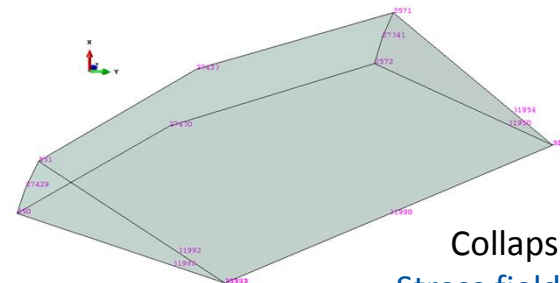
Global model:  
Modal Superposition Analysis



FE mesh of the crack front



Submodel:  
Quasi-static Analysis



Collapsed brick element:  
Stress field singularity modeling



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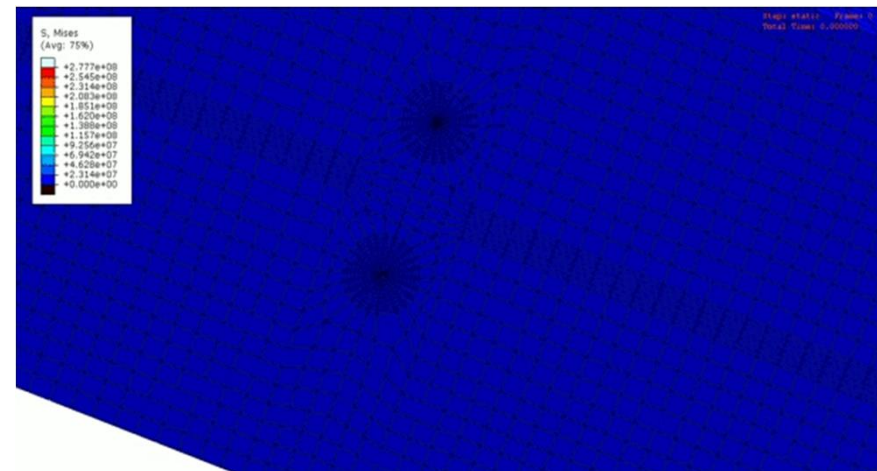
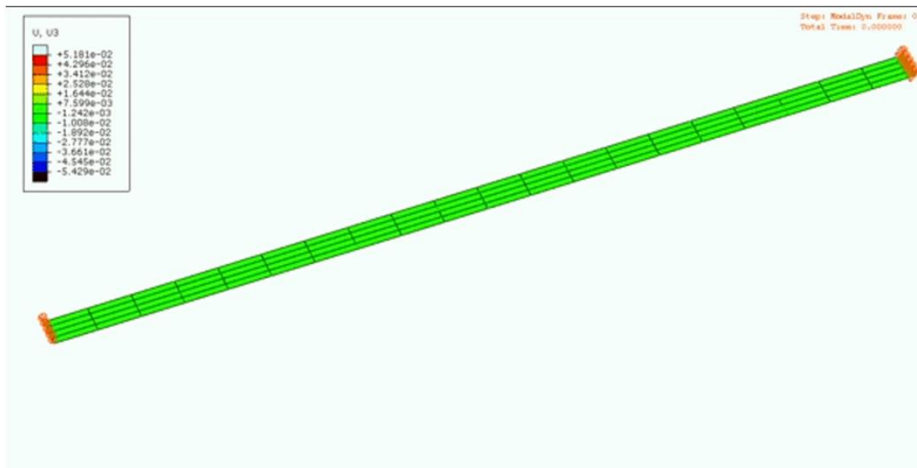
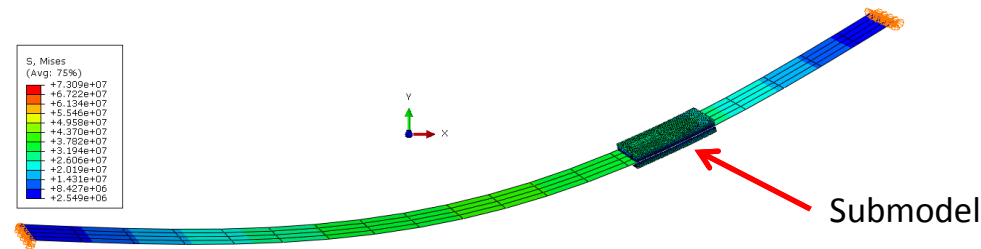


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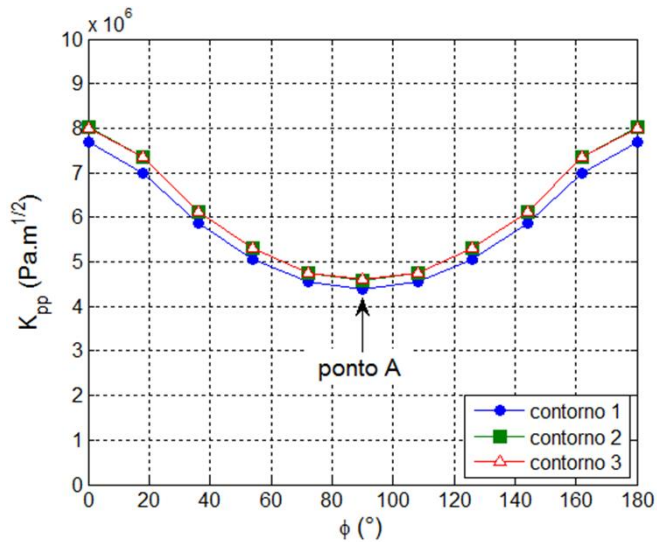


# A modeling methodology for global/local analysis

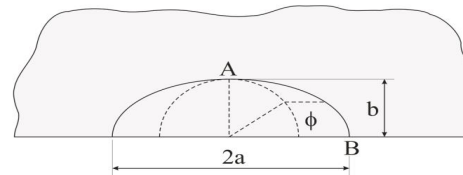
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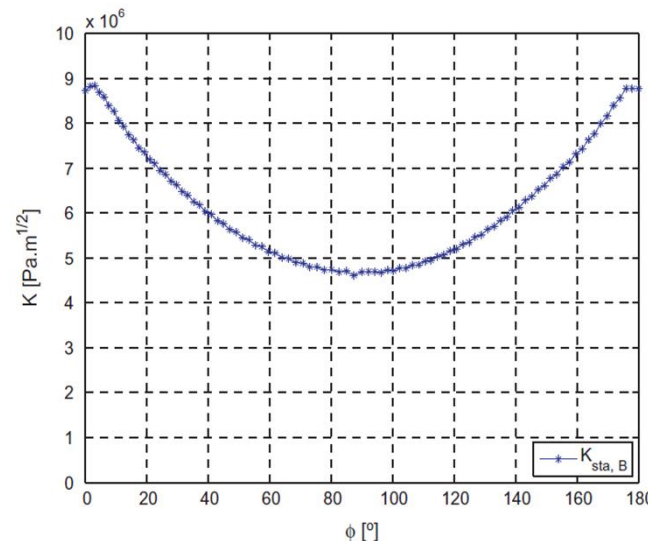


➤ Global/local approach used  
 SIF extraction method: J-integral



Dead load effect

$$K(t) = K_{static} + K_{dynamic}(t)$$



➤ Determined by  
 ALBUQUERQUE; DE CASTRO;  
 CALÇADA (2012)

SIF extraction method: VCCT





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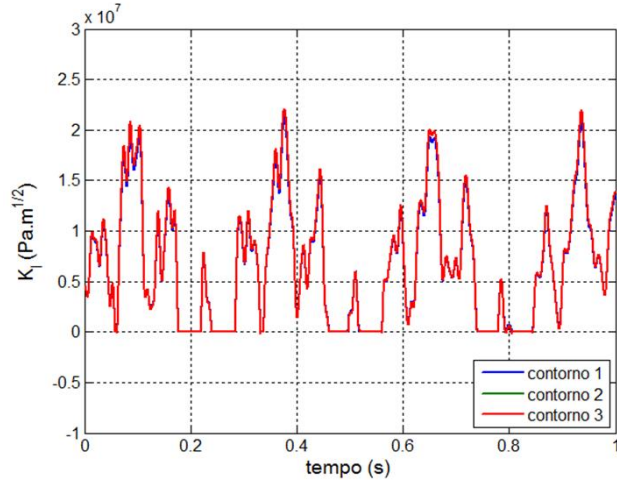
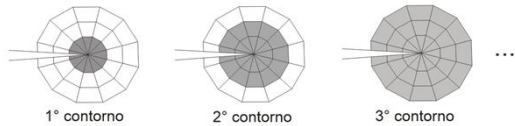


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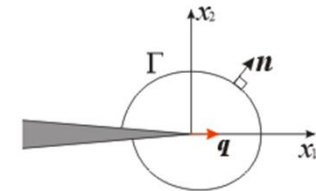
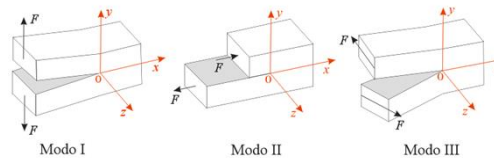
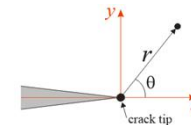
➤ Application: fatigue crack growth analysis of bridges

Fracture Mechanics: extraction of Dynamic Stress Intensity Factors

$$\sigma_{ij}(t) = \frac{K_I(t)}{\sqrt{2\pi r}} f_{ij}^I(\theta) + \frac{K_{II}(t)}{\sqrt{2\pi r}} f_{ij}^{II}(\theta) + \frac{K_{III}(t)}{\sqrt{2\pi r}} f_{ij}^{III}(\theta)$$

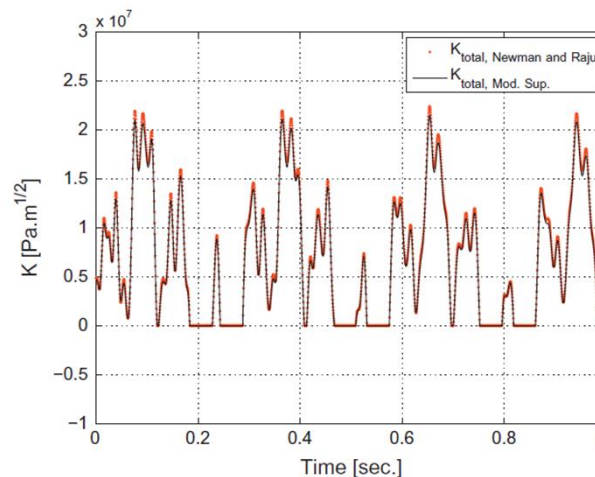


➤ Global/local approach used  
SIF extraction method: J-integral



$$J = \lim_{\Gamma \rightarrow 0} \int_{\Gamma} \left[ W \cdot \delta_{1j} - (\sigma_{ij} \cdot n_j) \cdot \frac{\partial u_i}{\partial x_1} \right] d\Gamma$$

$$J = \frac{K_I^2}{E^*} + \frac{K_{II}^2}{E^*} + \frac{K_{III}^2}{2G^*}$$



➤ Determined by ALBUQUERQUE; DE CASTRO; CALÇADA (2012)

SIF extraction method: VCCT

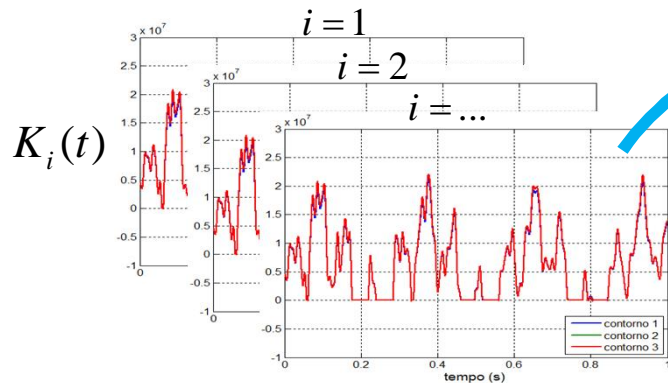




# A modeling methodology for global/local analysis

➤ Application: fatigue crack growth analysis of bridges

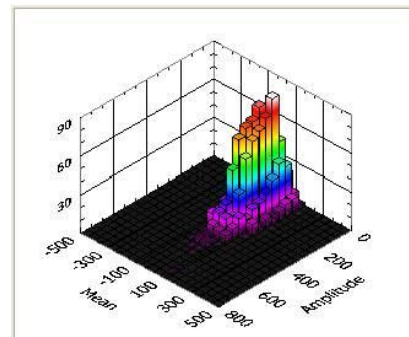
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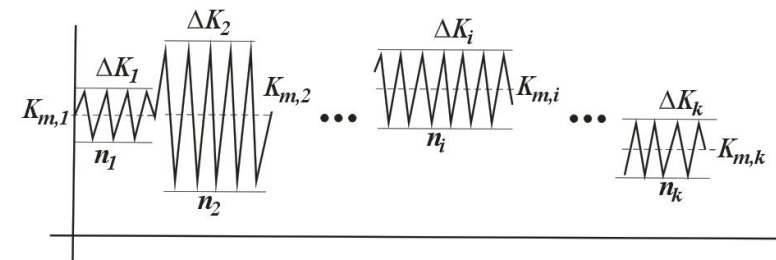
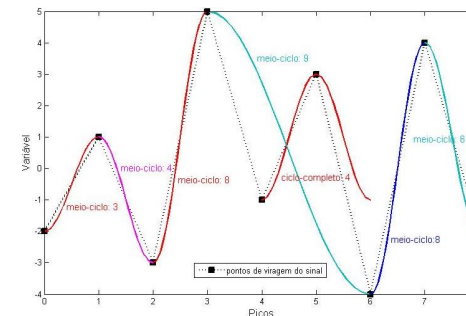
SIF histories: train sequences

$$\Delta K_{eq,i}$$

SIF spectrum



Rainflow counting





# A modeling methodology for global/local analysis

## ➤ Application: fatigue crack growth analysis of bridges

Fracture Mechanics: extraction of  
 Dynamic Stress Intensity Factors

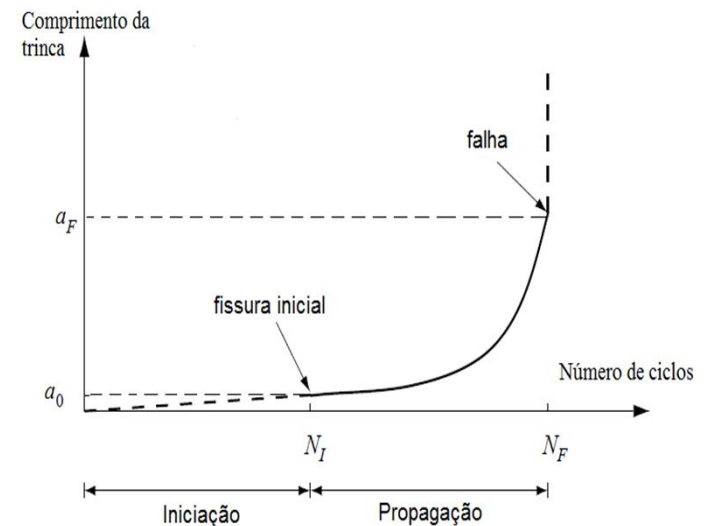
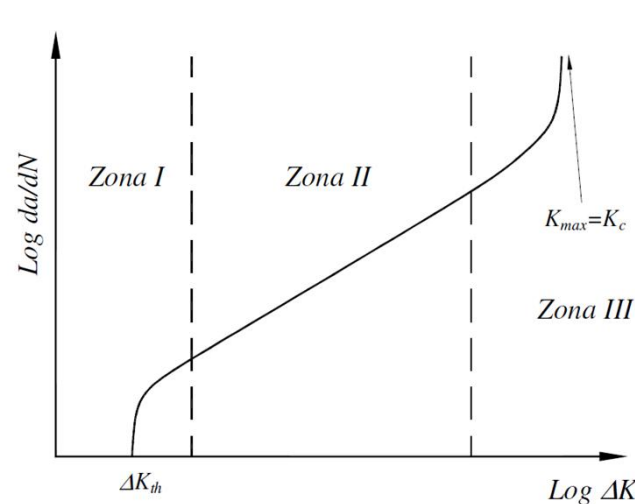
Comments:

- Stress Intensity Factor Time-Histories are important for assessing the residual life of the bridge when the fatigue crack growth approach is used;
- The Paris Law can be used to predict crack growth as a function of cycles;

Paris Law

$$\left. \frac{da}{dN} \right|_i = C \cdot \Delta K_{eq,i}^m$$

where  $N$  = number of cycles





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# Bridge simulation for fatigue analysis



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Universidade de São Paulo  
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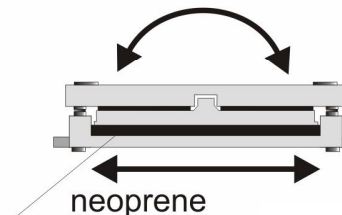
## Fatigue damage analysis of an old through-truss bridge



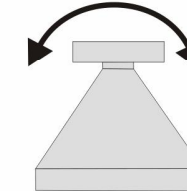
west bearing



east bearing



neoprene



Fundão River Bridge  
Unballasted through-truss bridge : 70-year old  
Span length: 41 m  
The bridge is part of the Vitória-Minas Railroad

The structure was designed in 1943  
according to AREMA (1941) specification







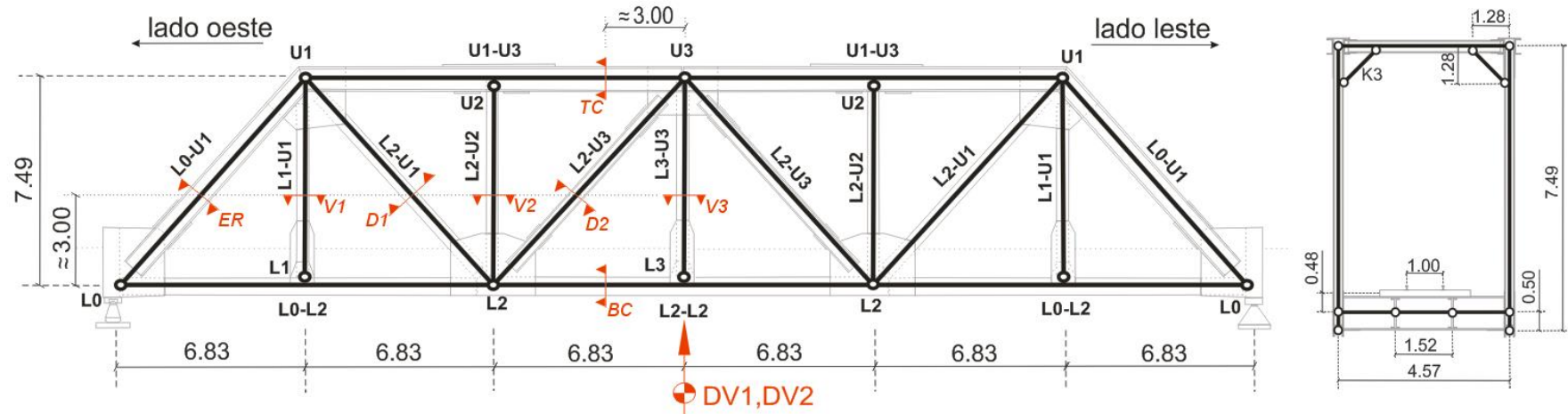
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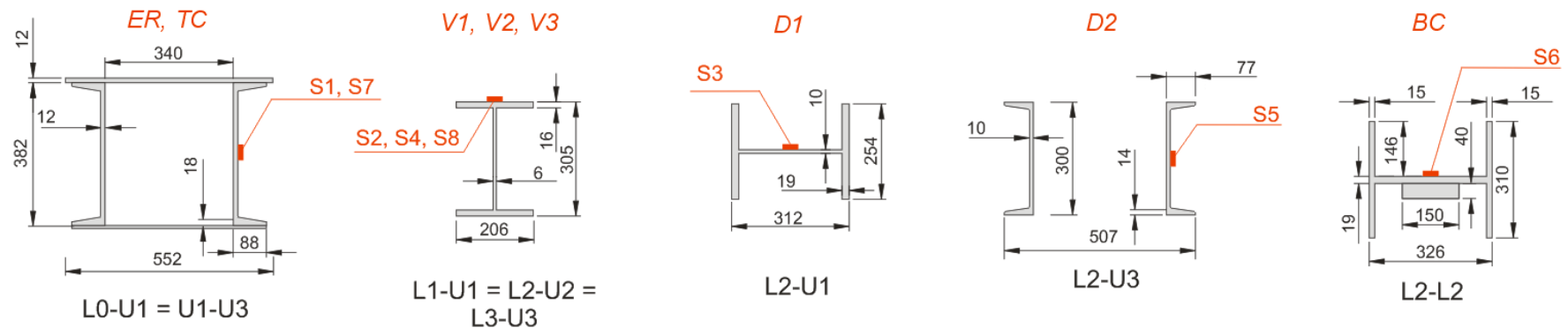
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# Fatigue damage analysis of an old through-truss bridge



(a) dimensões em m



(b) dimensões em mm





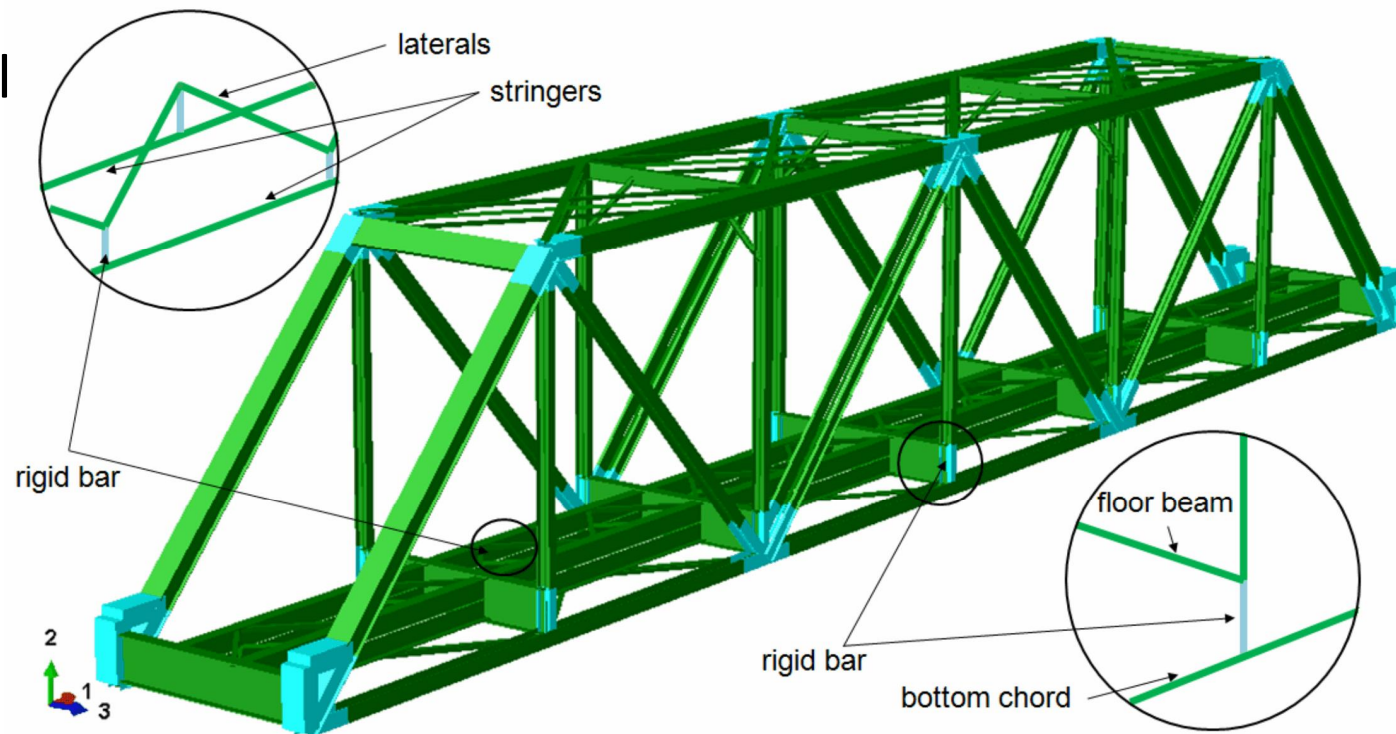
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# Fatigue damage analysis of an old through-truss bridge

Global model



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Universidade de São Paulo  
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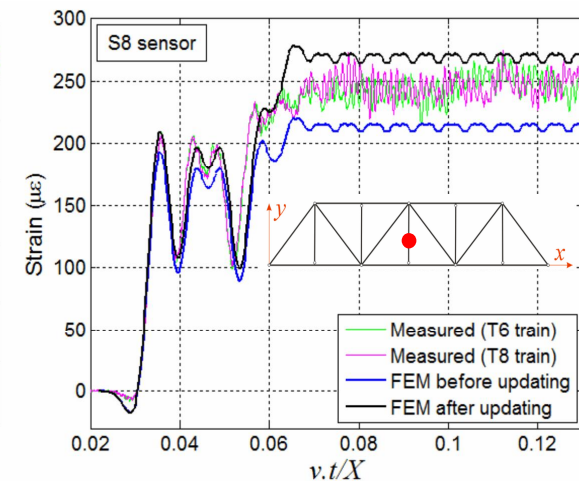
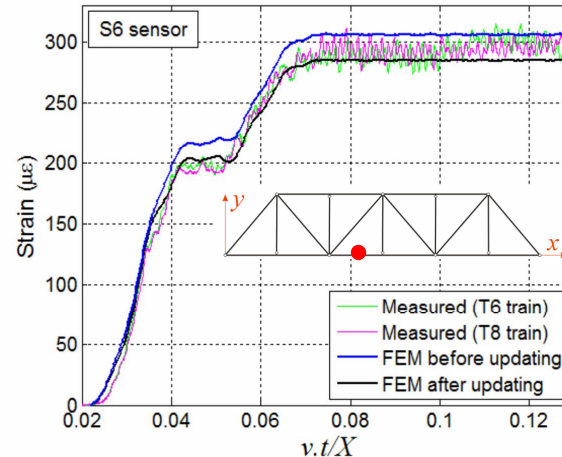
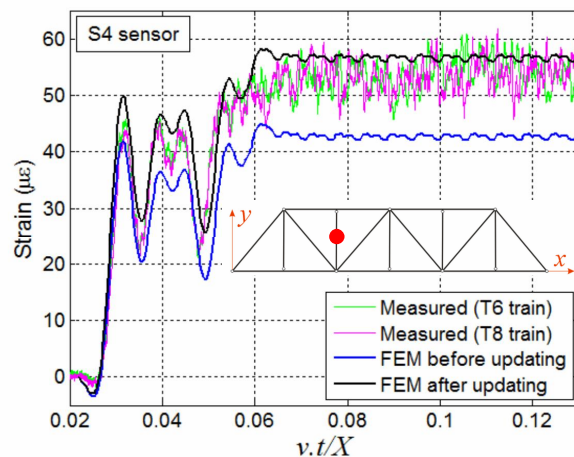
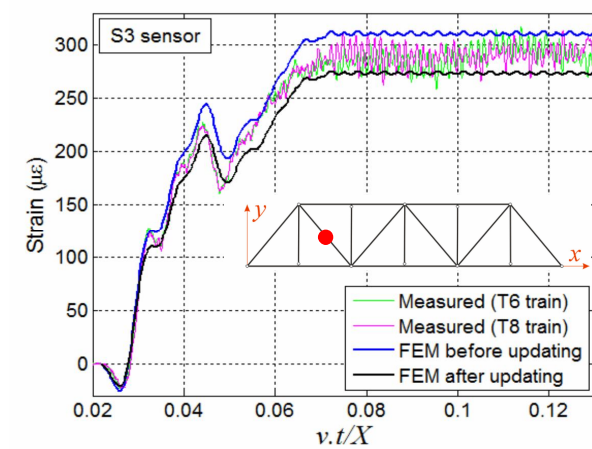
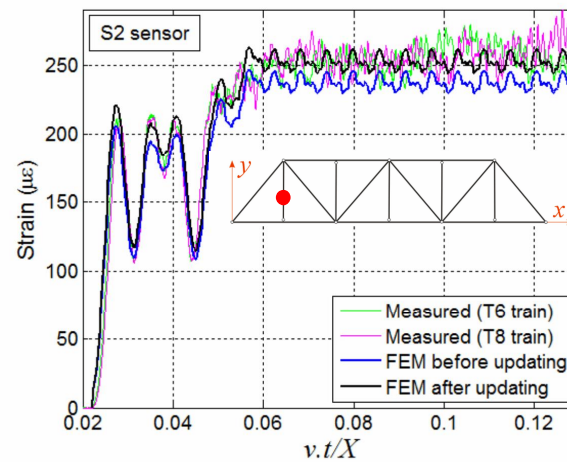
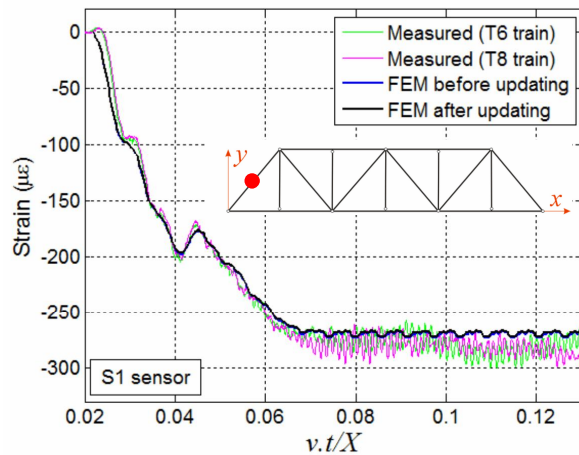
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# Fatigue damage analysis of an old through-truss bridge

Quasi-static analysis x Experimental results





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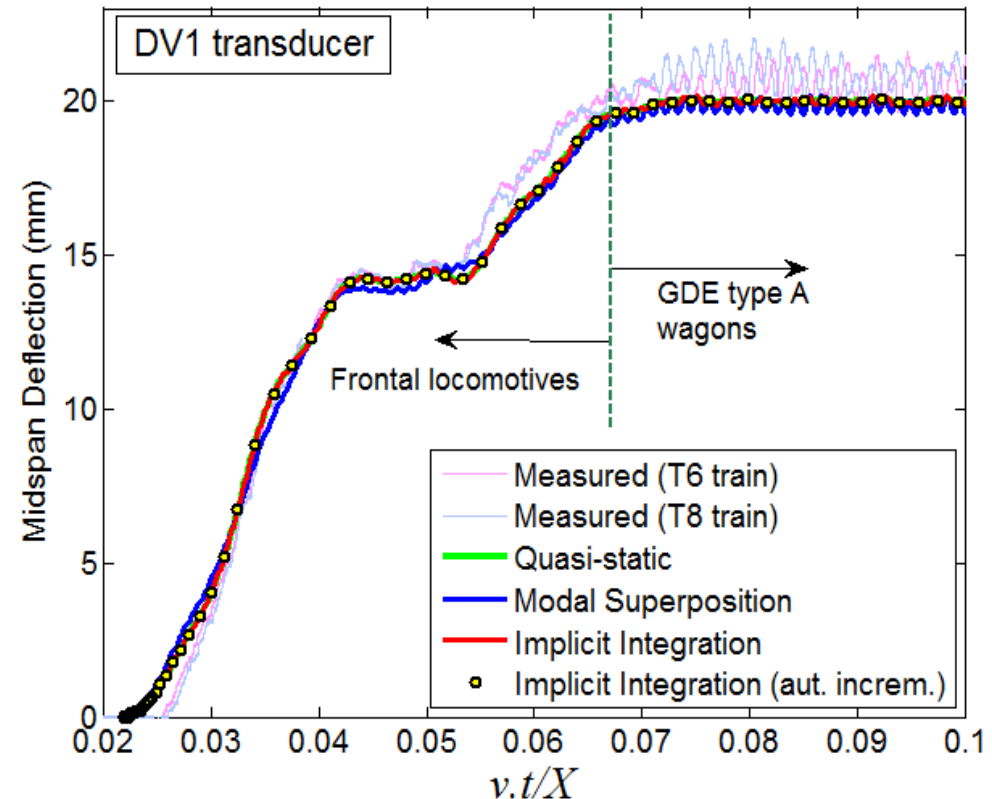
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# Fatigue damage analysis of an old through-truss bridge

*Comparisons between analysis procedures and experimental results*

Speeds between 24 km/h and 31 km/h were detected during monitoring



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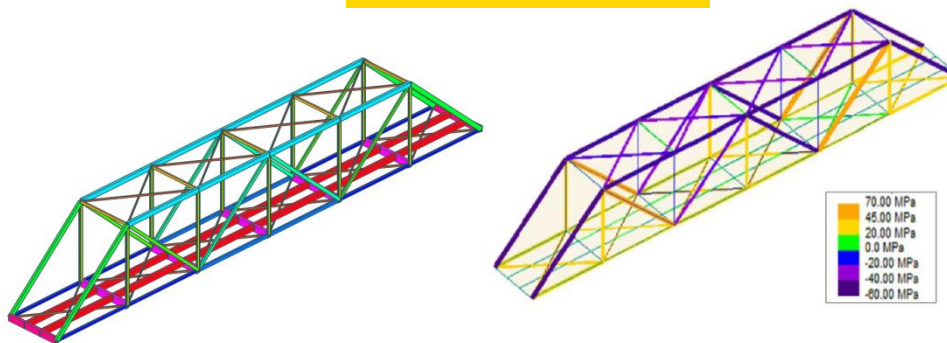


# The case of the Suaçui river bridge - VM railroad

Contribution EPFL



## Structural safety



$$n = \frac{R_d}{E_d} = 1.90$$

Diagonals

$$n = \frac{R_d}{E_d} = 2.11$$

Longitudinal girders

Degree of compliance

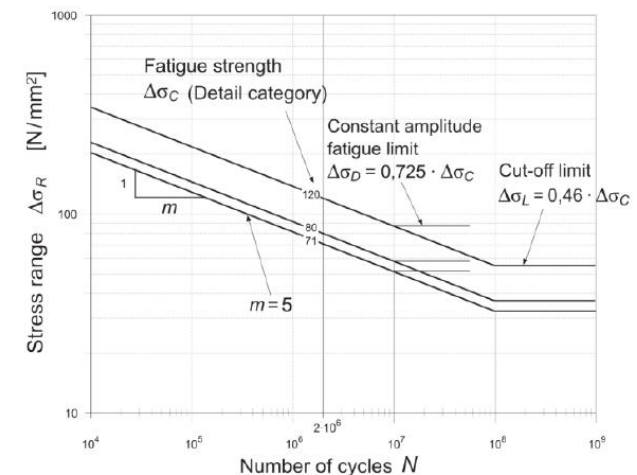
The calculation is based on 200 full GDE wagons for the full ore trains

## Fatigue Analysis

Fatigue scenario with approximately 8740 trains per year.

S-N curve occurring to the fatigue category 80 and 71 for truss and deck member.

The members were found to have sufficient capacity even for another 50 years.



S-N curve used in study (SIA 269/3, 2011).





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# Methodologies of Dynamic Analysis of Bridges for High Speed Trains



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Universidade de São Paulo  
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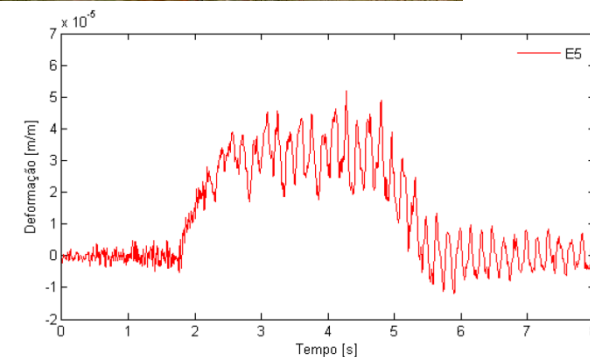
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## Methodologies of Dynamic Analysis of Bridges for High Speed Trains

➤ Technological developments in the rail transport sector has led to the development of new trains capable of speeds of circulation exceeding 200 km/h .

➤ This increase in speed railways poses new challenges in the structural design of bridges , emphasizing the dynamic behavior, where the vibrations induced by the passage of rail traffic cause in general, displacements and internal forces in the structure significantly greater than that produced by the application of static load so as to pose in risk the structural safety of the bridge

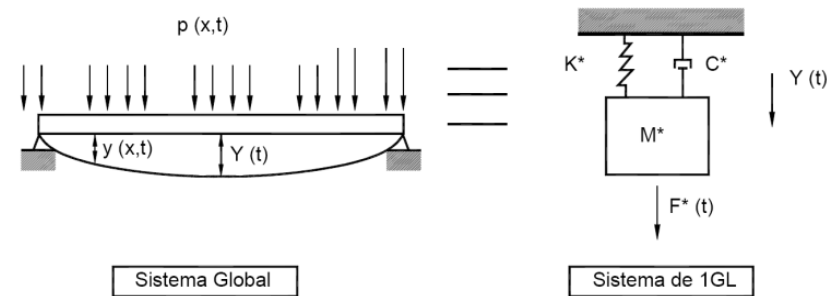




## Simplified methodologies

Easy to use and implement in commercial programs. This method is suitable for cases in which interaction does not significantly influence the dynamic response of the structure:

- ✓ Decomposition of Excitation at Resonance method (DER).
- ✓ Dynamic influence line calculation method (LIR).



$$M^* \ddot{Y}(t) + C^* \dot{Y}(t) + K^* Y(t) = F^*(t)$$

Where:

$M^*$ : Mass generalized,  $C$ : Damping generalized,  
 $K$ : Stiffness generalized,  $F^*$ : Force generalized.



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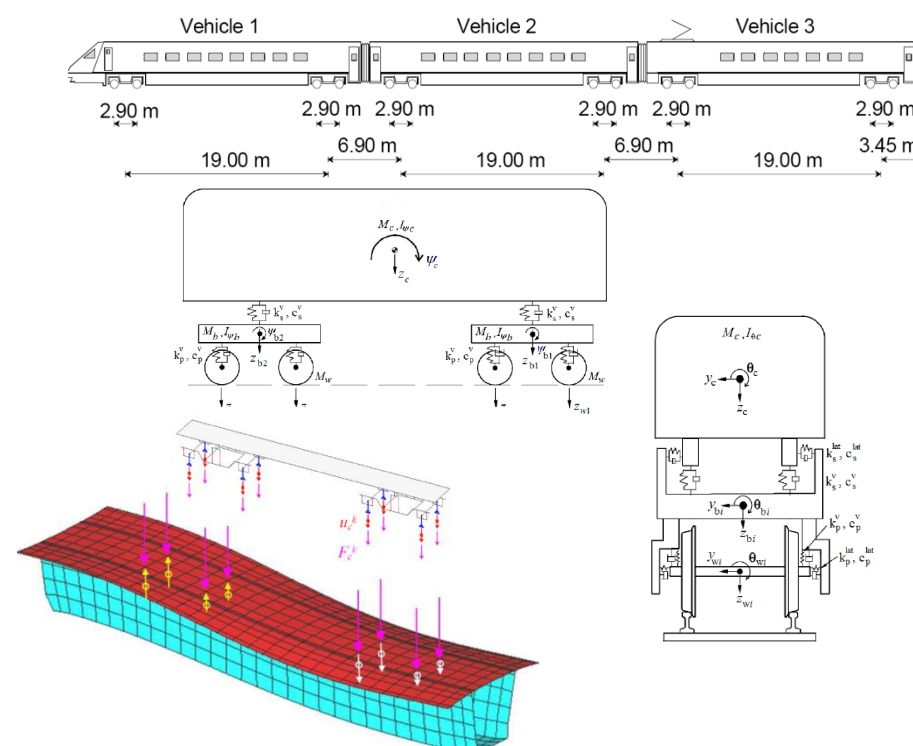


## Sophisticated methodologies

More difficult to use because it involves modeling the train and the knowledge of their parameters, is not directly available in commercial calculation programs.

This methodology is very relevant in situations where one wishes to evaluate:

- ✓ The comfort of passengers.
- ✓ Analyze the stability of the wheel-rail contact.
- ✓ Evaluate the effects of track irregularities.







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## Application of simplified methodologies

The evaluation of dynamic response is applied to a bridge formed by simply supported spans with the following characteristics:

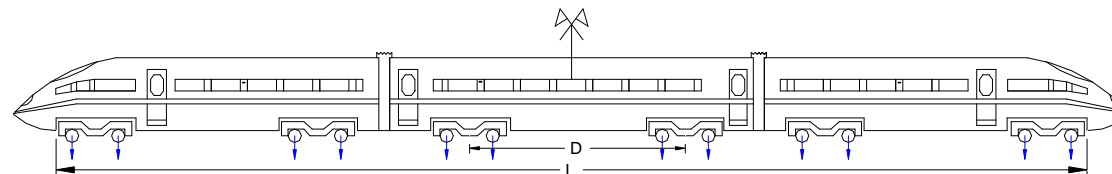
$L = 15\text{m}$

$EI = 7694 \times 103 \text{ kN.m}^2$

Mass:  $m = 15 \text{ t/m}$

damping  $\xi = 2\%$

Two types of trains are considered to cross the above bridge: Eurostar and TGV circulating at speeds between 140-420 km/h with increments of speed of 10 km/h.



Train	Type of Train	Length L (m)	Distance (D) between wagons (m)	Axle Load (kN)
TGV atlantique	Articulate	468,14	18,7	170
Eurostar	Articulate	386,67	18,7	170
Talgo AV2	Regular	356,05	13,14	170



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## Application of simplified methodologies

### ➤ Direct Integration method and Modal Superposition method

- ✓ The dynamic response calculation by these methods has been carried out in the SAP2000 program taking advantage of the Time-History module;
- ✓ The iterative process has been implemented in MatLab, the management of SAP2000 files is possible through APIs, the analysis is automatic and allows an efficient data storage and manipulation;
- ✓ In the following figures, a comparison of results (deflections and accelerations) obtained by different methods for different speeds is presented.



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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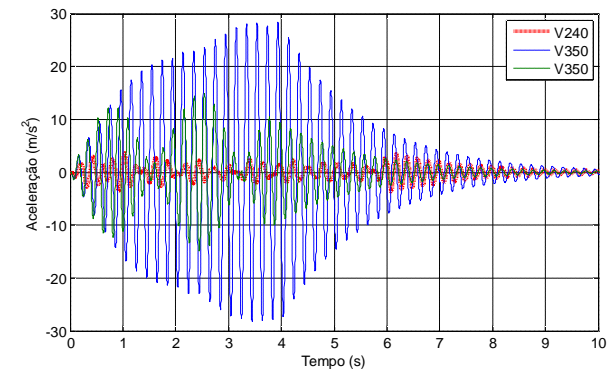
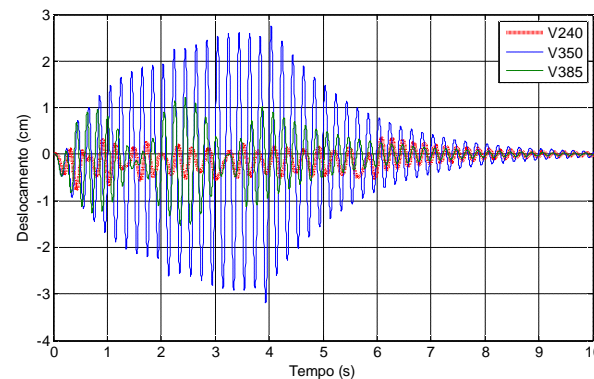
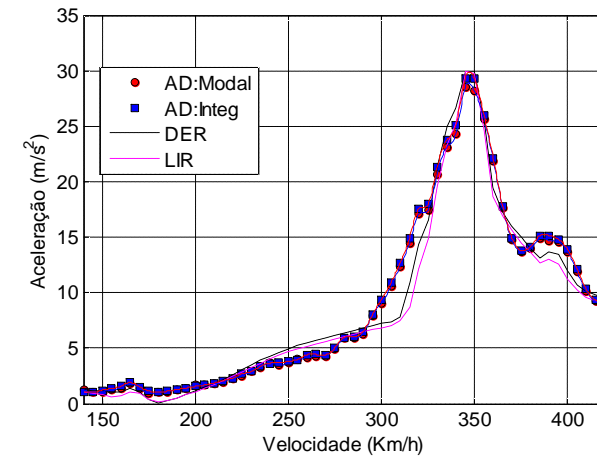
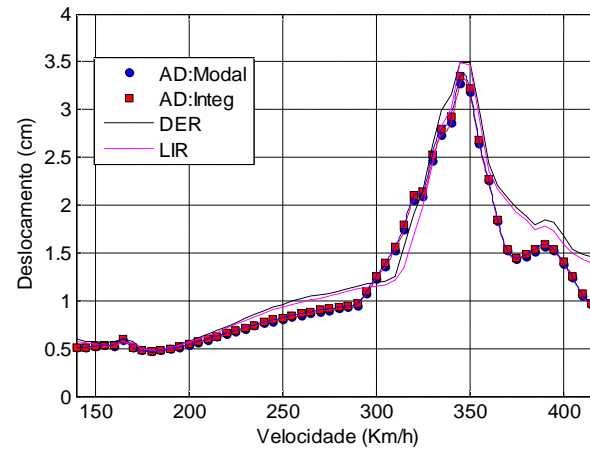
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# Application of simplified methodologies

➤ Eurostar train:





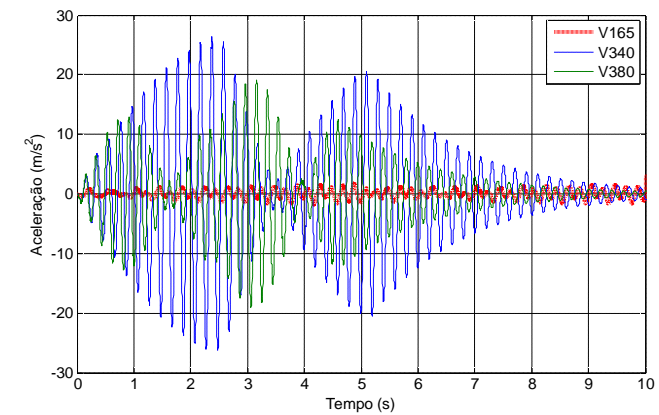
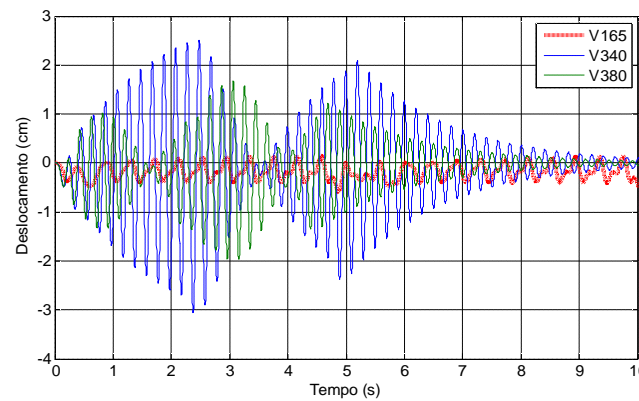
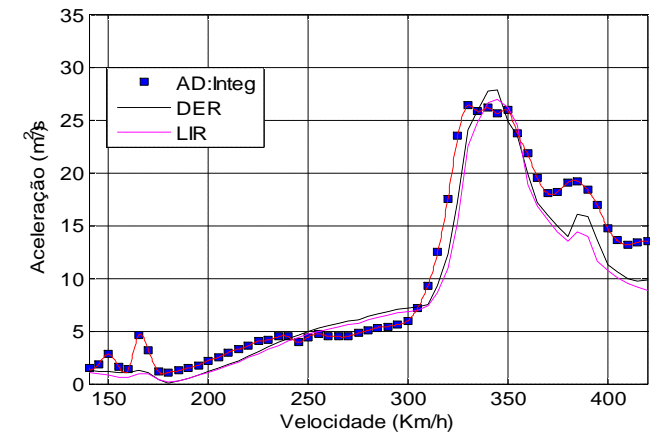
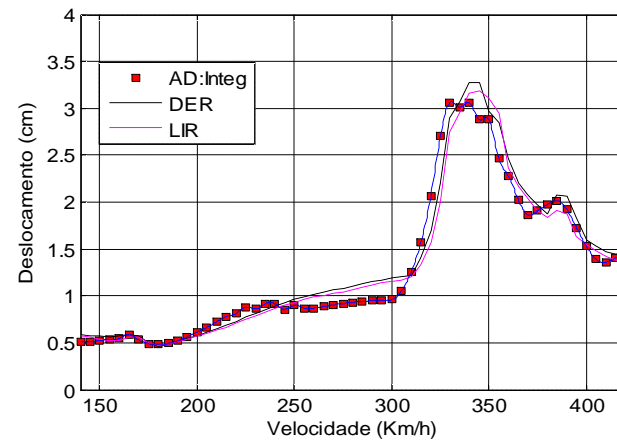
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# Application of simplified methodologies

➤ TGV train:







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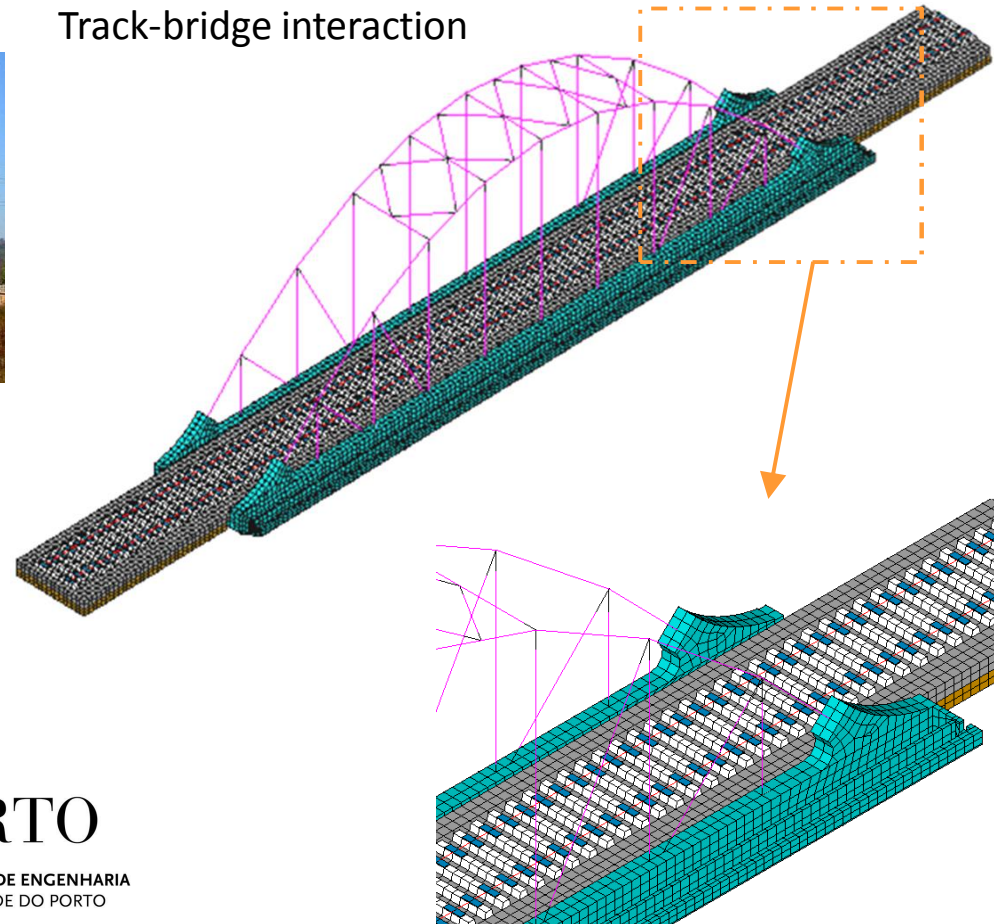
## Sophisticated Dynamic modeling of railway bridges

RIBEIRO et al. (2013)



Bridge over the São Lourenço River – span of 42 m  
Railway bridge of the Portuguese high speed system  
(220 km/h)  
In operation.

Track-bridge interaction



Finite Element Model in ANSYS FEA software

Courtesy: Prof. Rui Calçada - FEUP



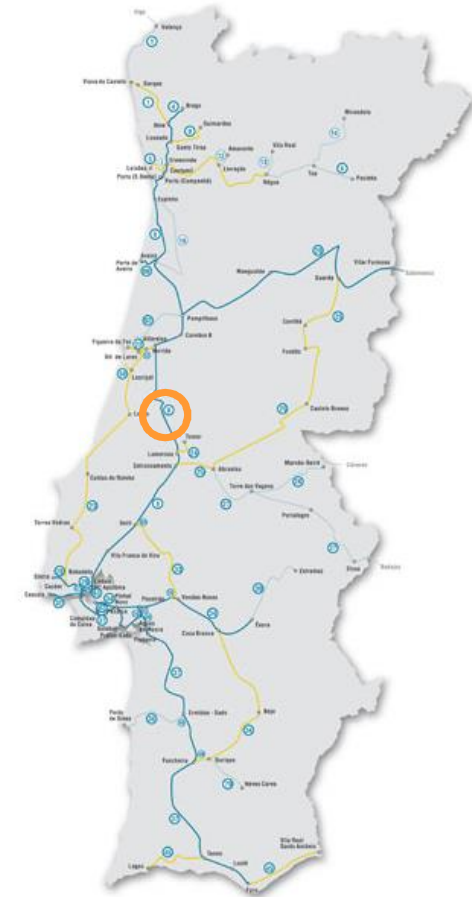
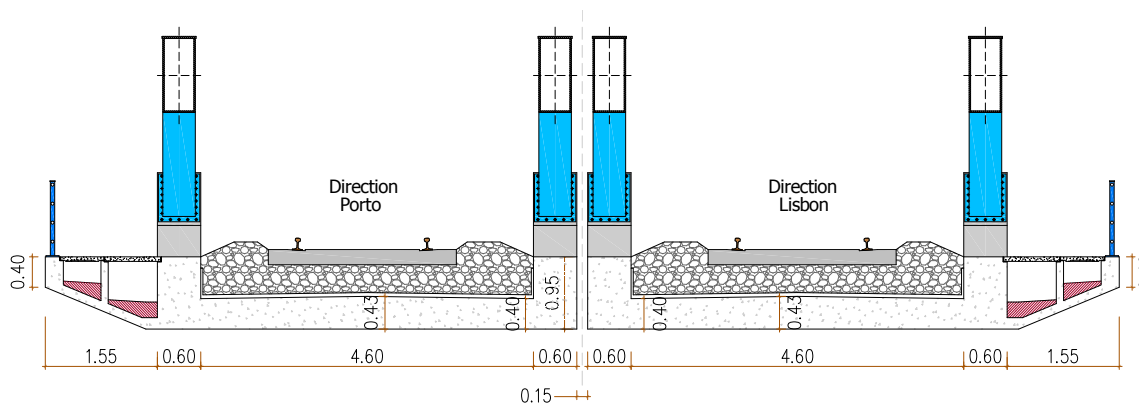


# Palestra: "Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes"

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## Description of the bridge





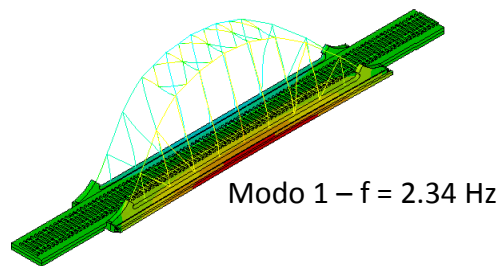
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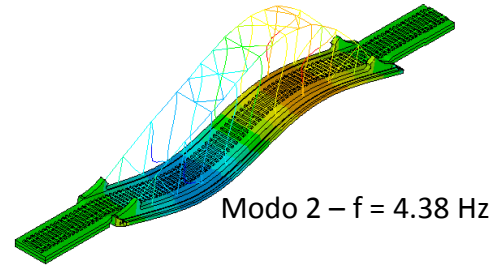


# Dynamic modeling of bridges in Portugal

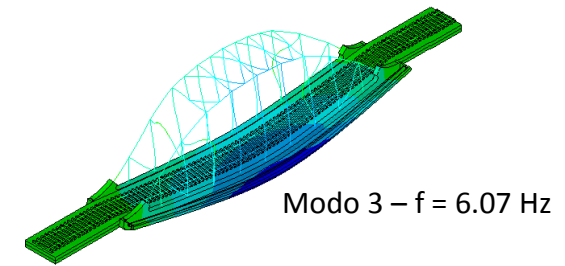
Courtesy: Prof. Rui Calçada - FEUP



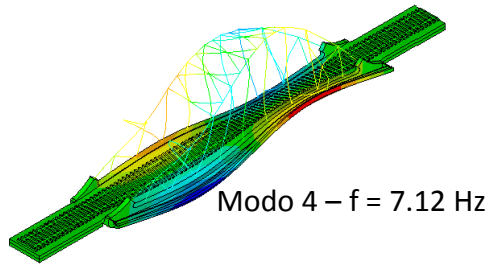
Modo 1 –  $f = 2.34$  Hz



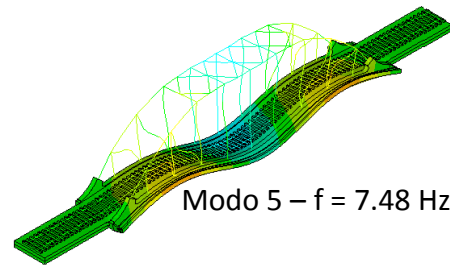
Modo 2 –  $f = 4.38$  Hz



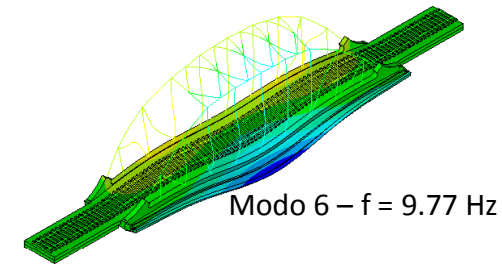
Modo 3 –  $f = 6.07$  Hz



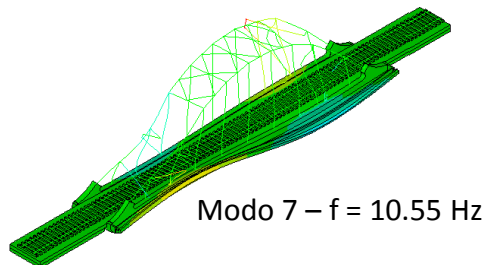
Modo 4 –  $f = 7.12$  Hz



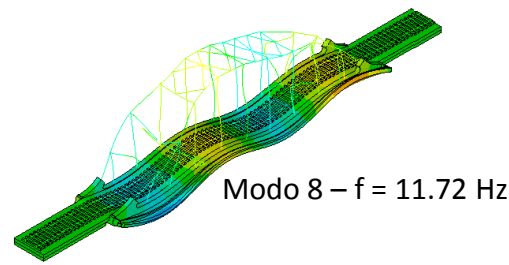
Modo 5 –  $f = 7.48$  Hz



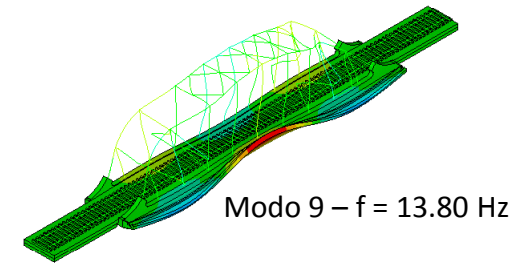
Modo 6 –  $f = 9.77$  Hz



Modo 7 –  $f = 10.55$  Hz



Modo 8 –  $f = 11.72$  Hz



Modo 9 –  $f = 13.80$  Hz



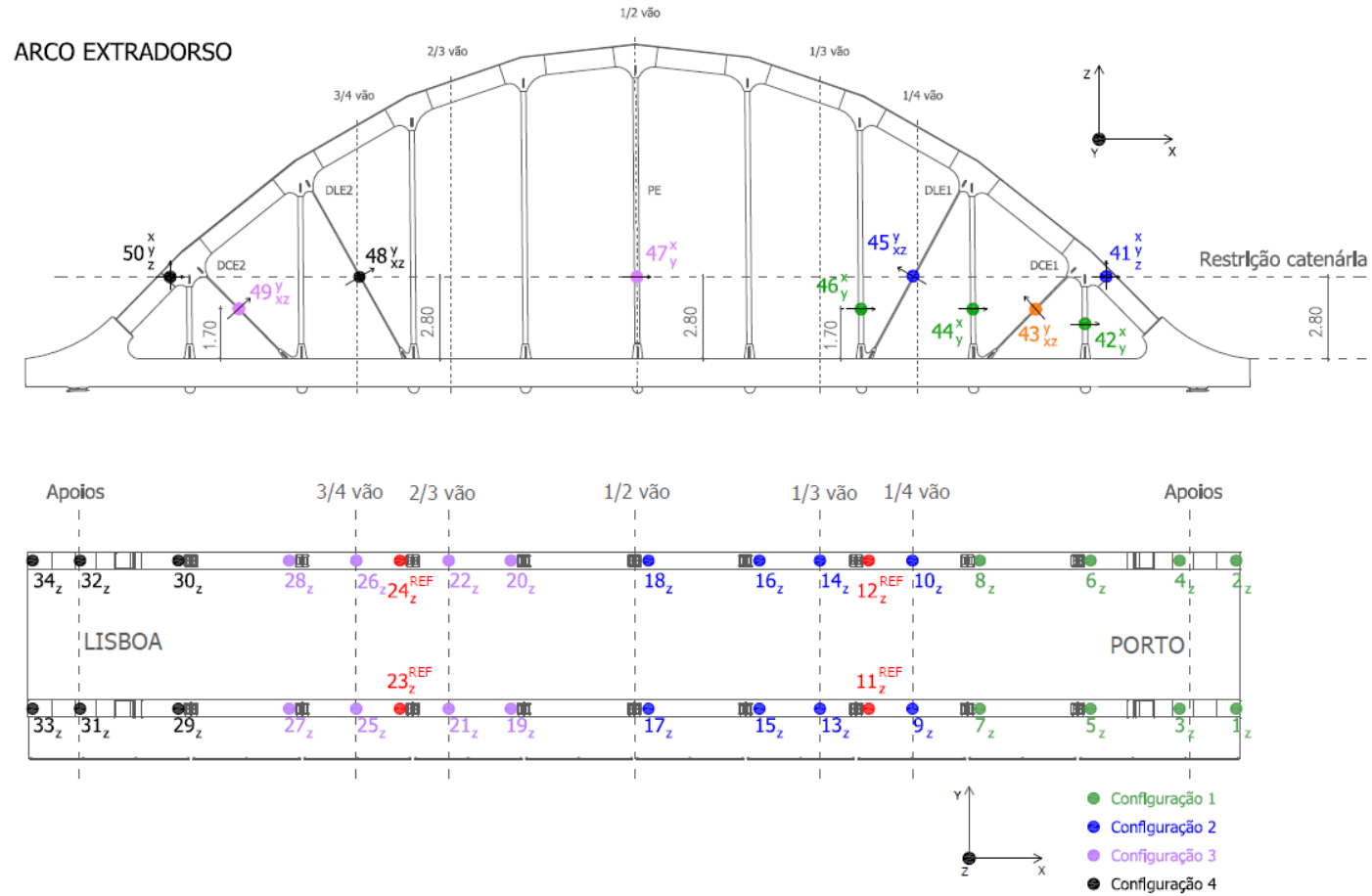


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## Modal parameters identification



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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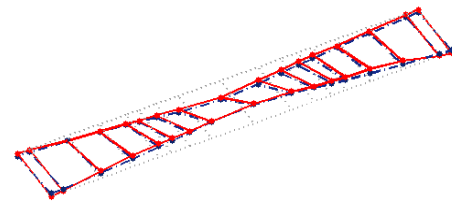
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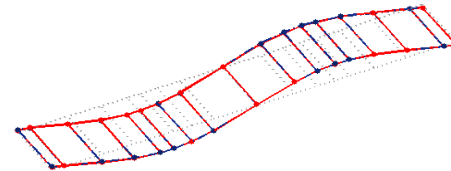


# Dynamic modeling of bridges in Portugal

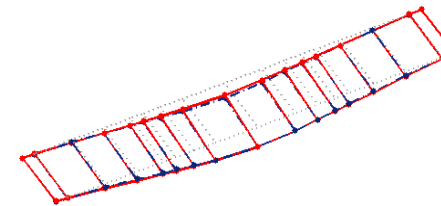
Courtesy: Prof. Rui Calçada - FEUP



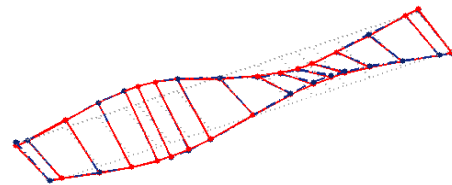
2.34 Hz    2.34 Hz    0.0 %



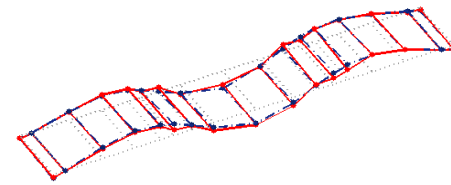
4.38 Hz    4.37 Hz    0.2 %



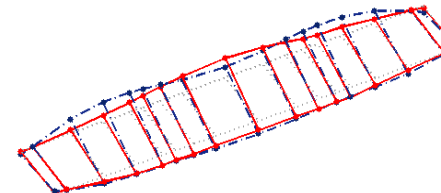
6.07 Hz    6.02 Hz    0.8 %



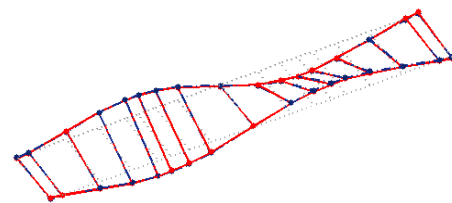
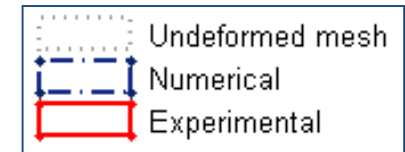
7.12 Hz    7.11 Hz    0.1 %



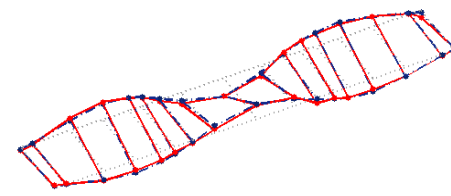
7.48 Hz    7.43 Hz    0.7 %



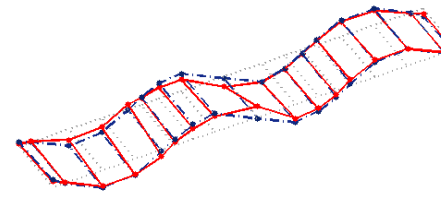
9.77 Hz    9.76 Hz    0.1 %



10.55 Hz    9.93 Hz    6.2 %



11.72 Hz    11.30 Hz    3.7 %



13.80 Hz    13.76 Hz    0.3 %

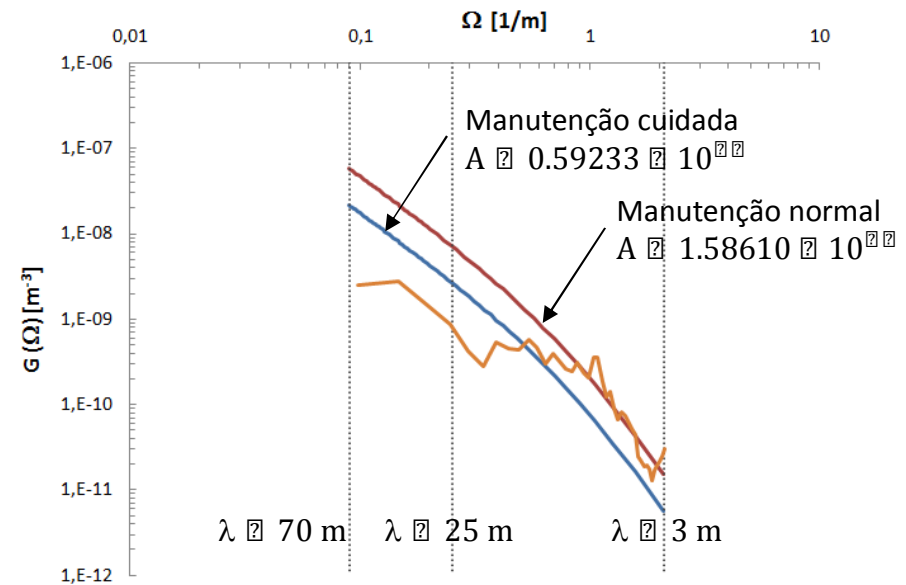
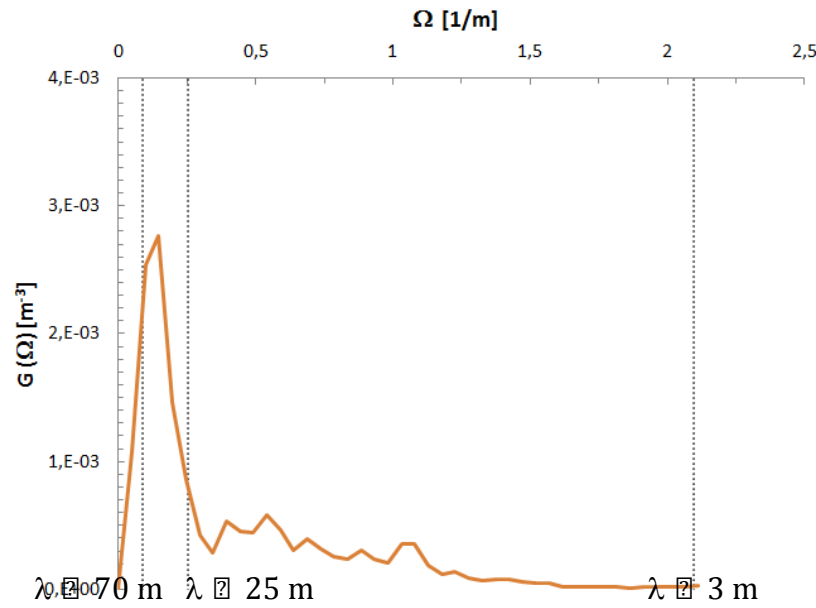
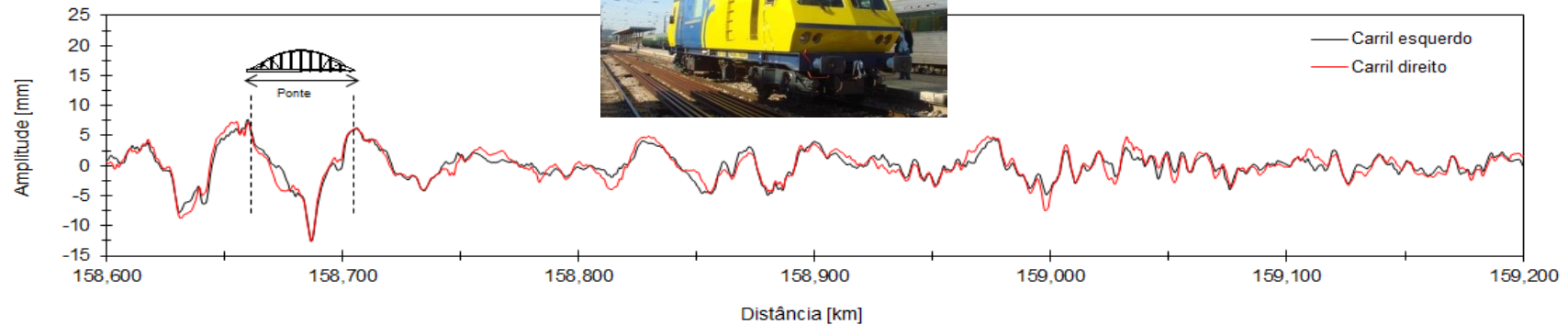


# Palestra: "Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes"

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## Railway Irregularities



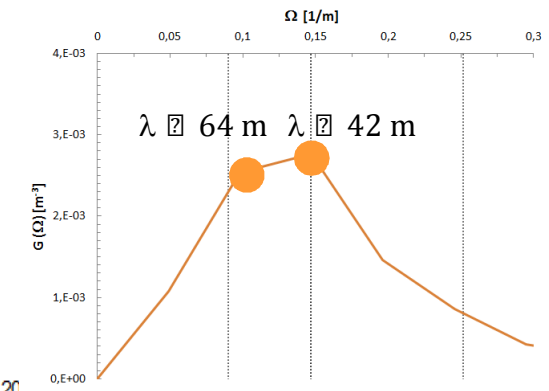
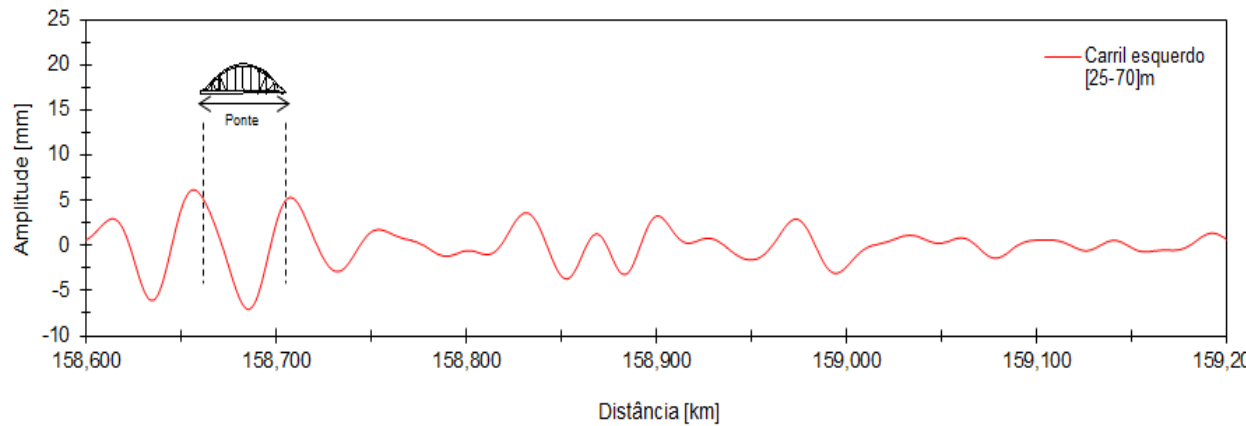
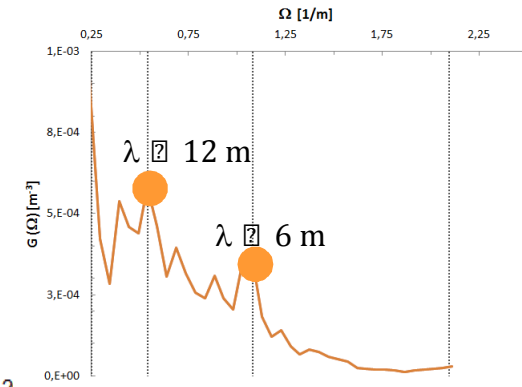
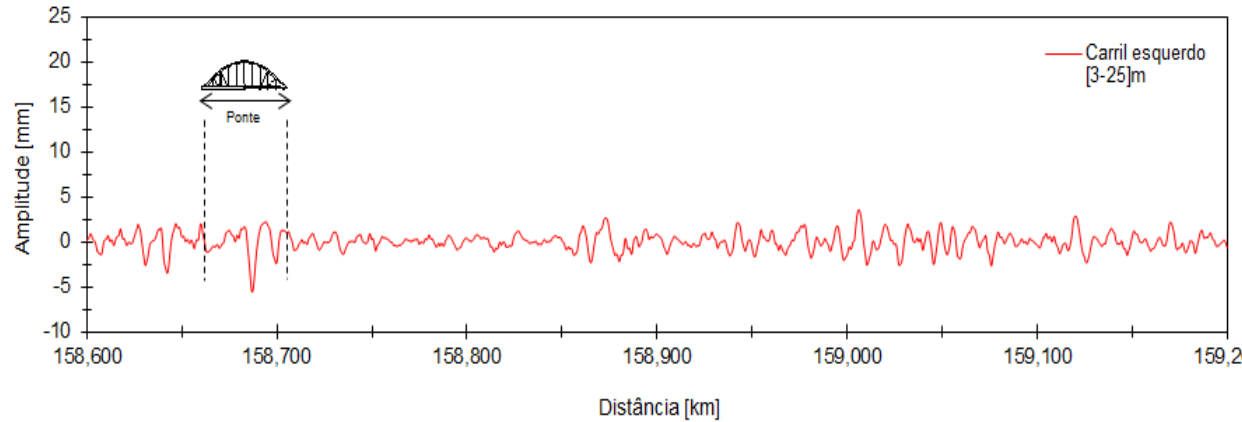


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## Railway Irregularities



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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## Dynamic Model of the Alfa pendular train



Distance between axles  $D = 25.9$  m

Axle Load  $P = 129-137$  kN

Total Length  $L = 158.9$  m

Maximum Speed  $v = 220$  km/h



Túlio N. Bittencourt  
Universidade de São Paulo  
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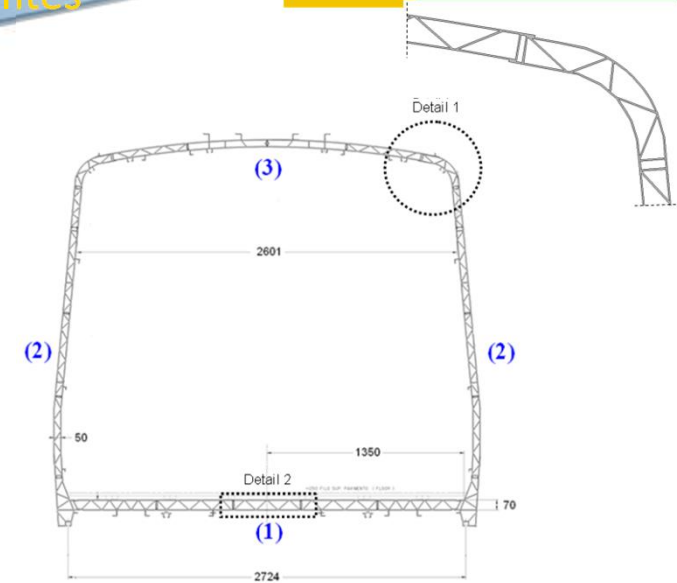
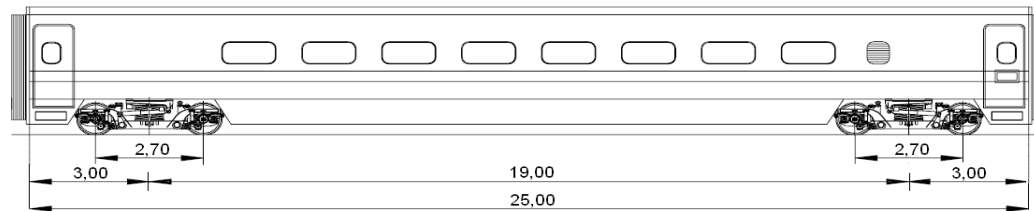


# Palestra: "Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes"

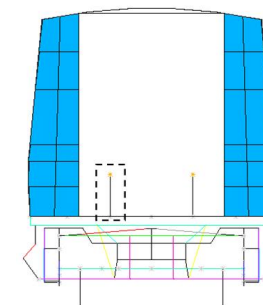
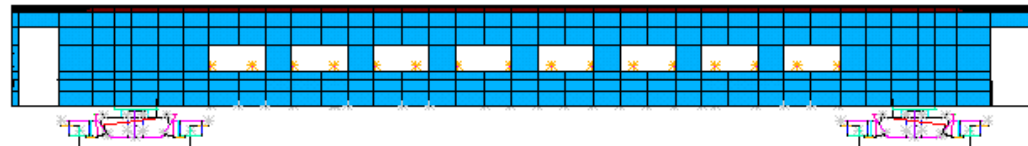
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## Finite Element Model



- (1) Base
- (2) Painéis laterais
- (3) Cobertura



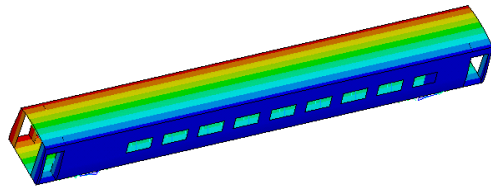


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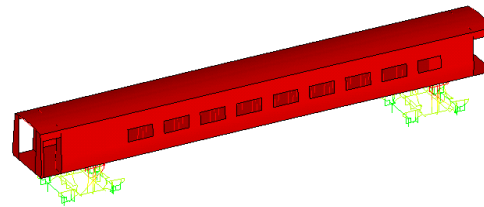
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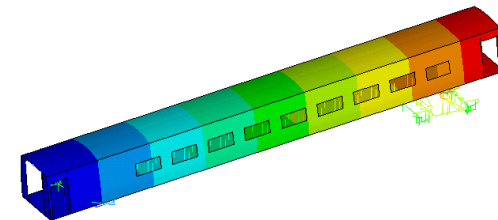
Computed Modal Parameters



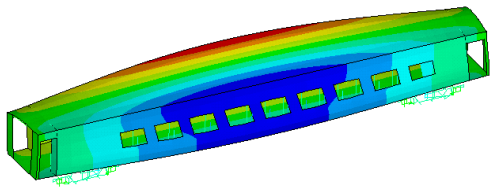
1C -  $f_D = 1.01$  Hz



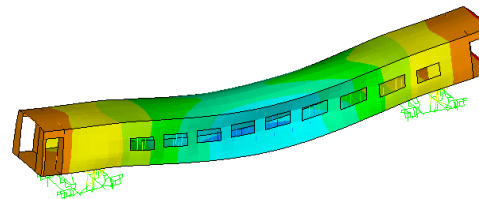
2C -  $f_D = 1.24$  Hz



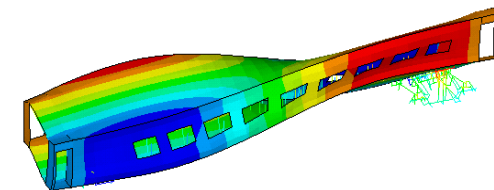
3C -  $f_D = 1.70$  Hz



4C -  $f_D = 8.39$  Hz



5C -  $f_D = 12.16$  Hz



6C -  $f_D = 17.73$  Hz





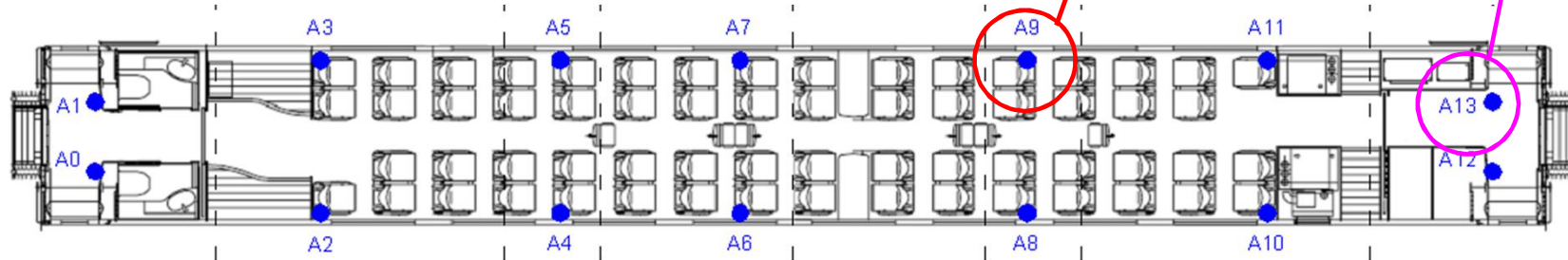
# Palestra: "Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes"



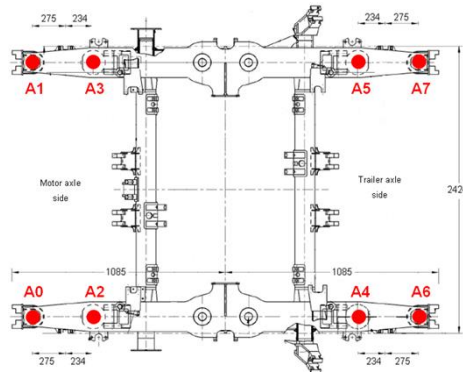
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## Modal Parameters Identification

### Wagon Instrumentation



### Truck Instrumentation





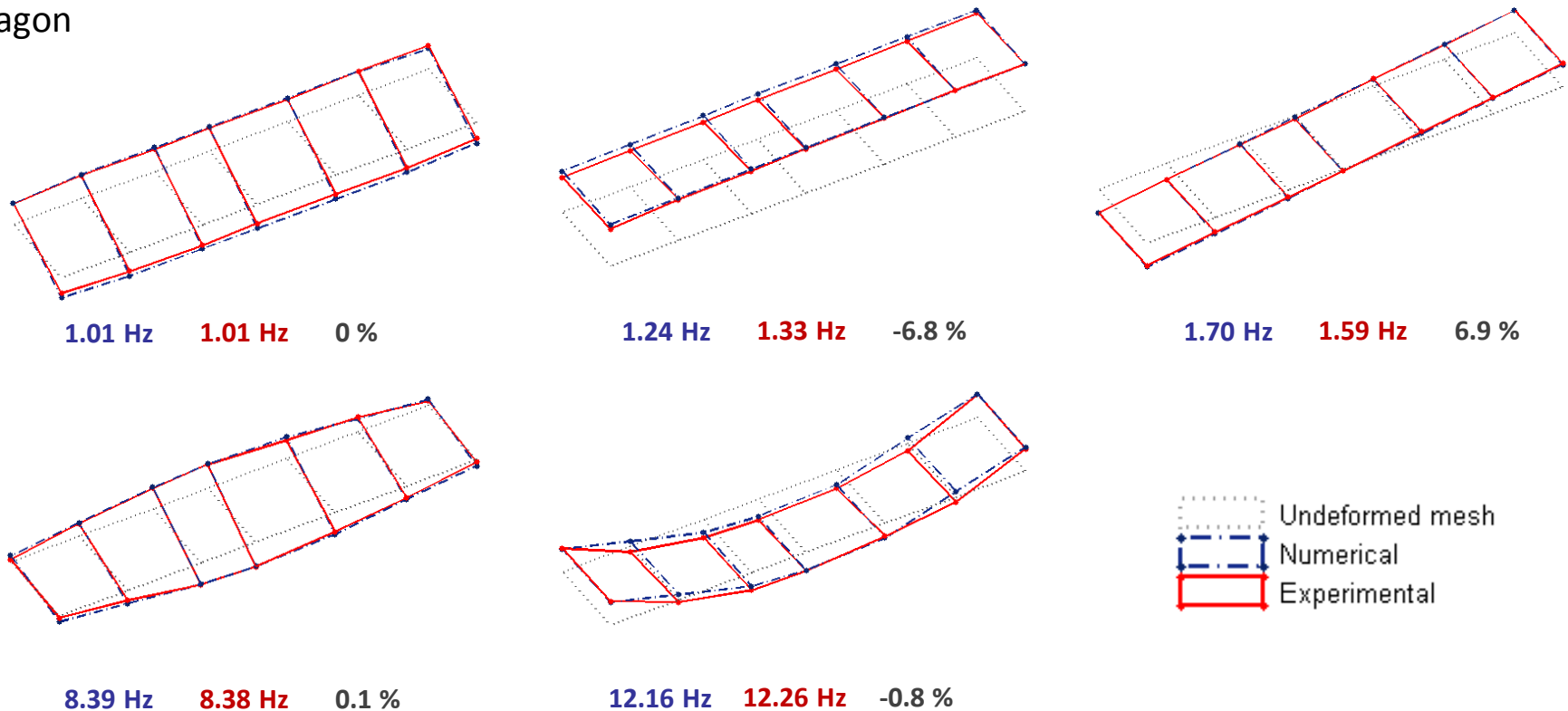
# Palestra: "Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes"



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## Numerical vs Experimental Modal Parameters

Wagon



D. Ribeiro, R. Calçada, R. Delgado, M. Brehm and V. Zabel. Finite element model calibration of a railway vehicle based on experimental modal parameters, Vehicle System Dynamics, Volume 51, Issue 6, 2013



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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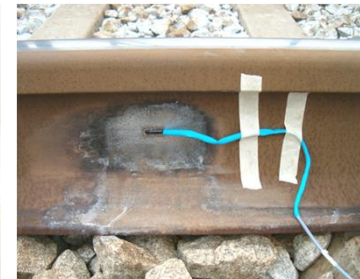
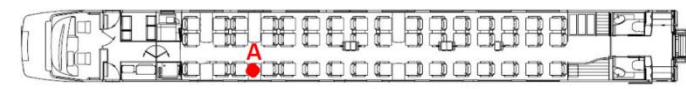
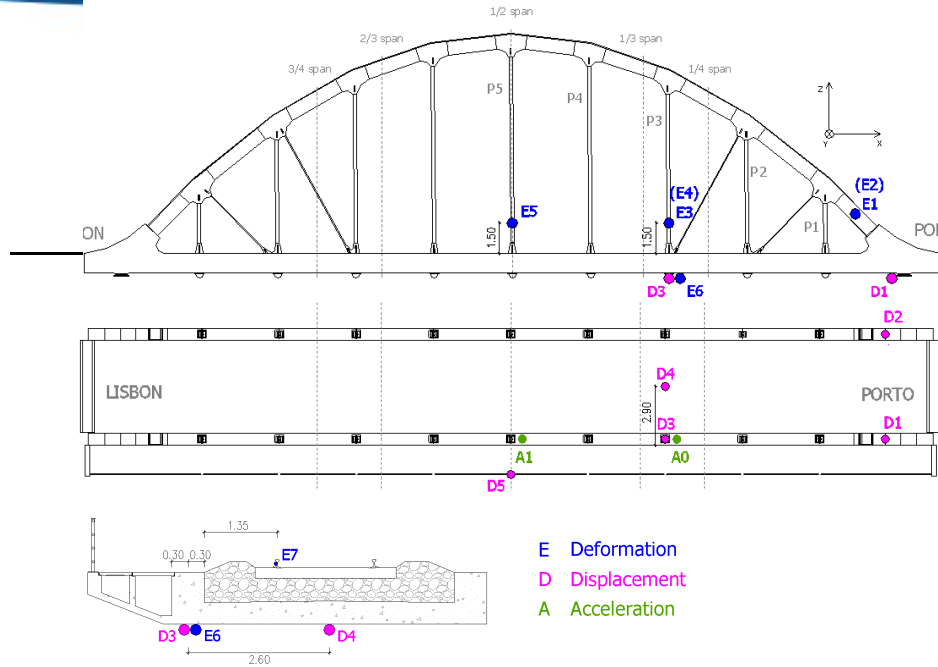


# Palestra: “Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes”

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## Dynamic Test under real traffic



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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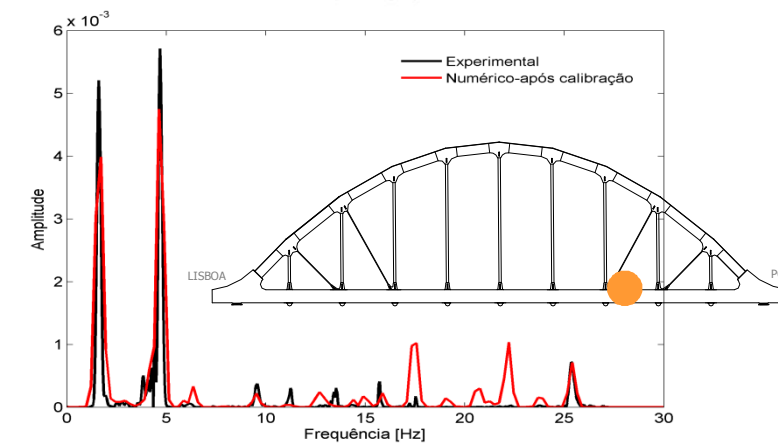
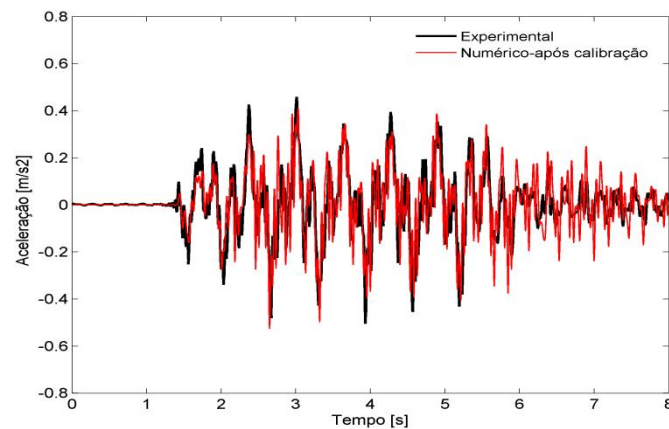
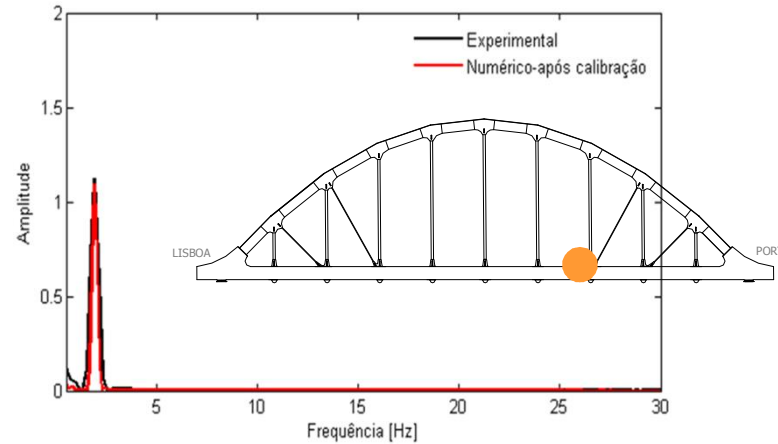
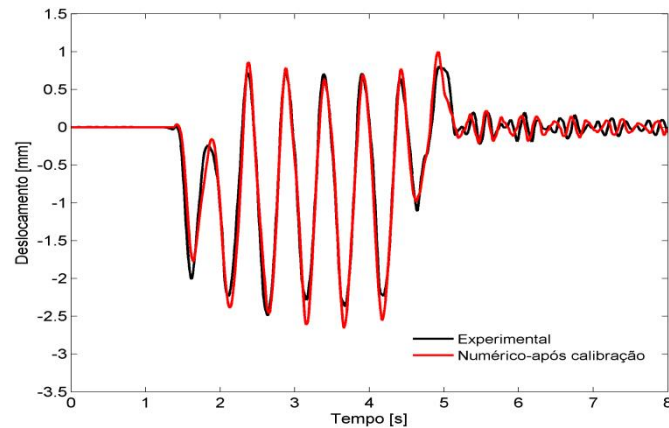


# Dynamic modeling of bridges in Portugal

Courtesy: Prof. Rui Calçada - FEUP



FEUP FACULDADE DE ENGENHARIA  
UNIVERSIDADE DO PORTO



Alfa pendular train  
( $v = 180 \text{ km/h}$ )



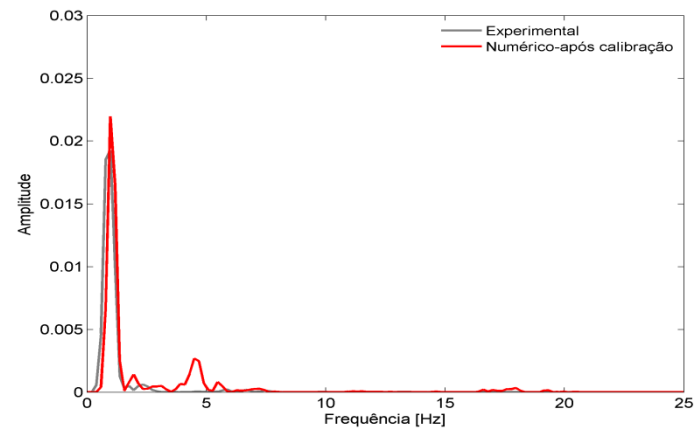
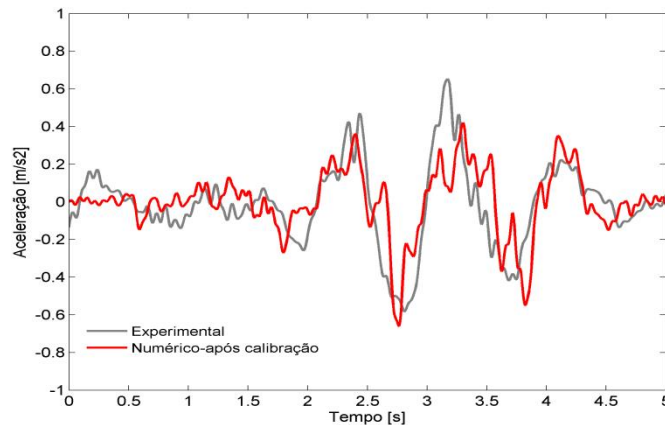
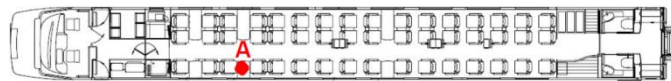
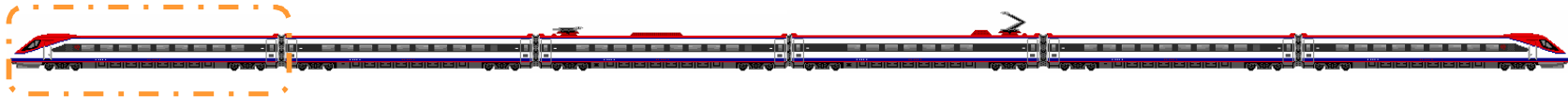
# Palestra: "Modelagem Computacional como Ferramenta para o Monitoramento de Estruturas de Pontes Existentes"



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## Dynamic Response under real traffic

Alfa pendular train ( $v = 180 \text{ km/h}$ )



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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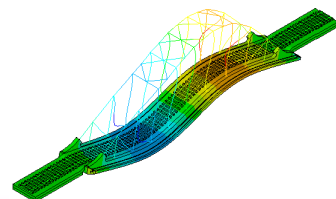
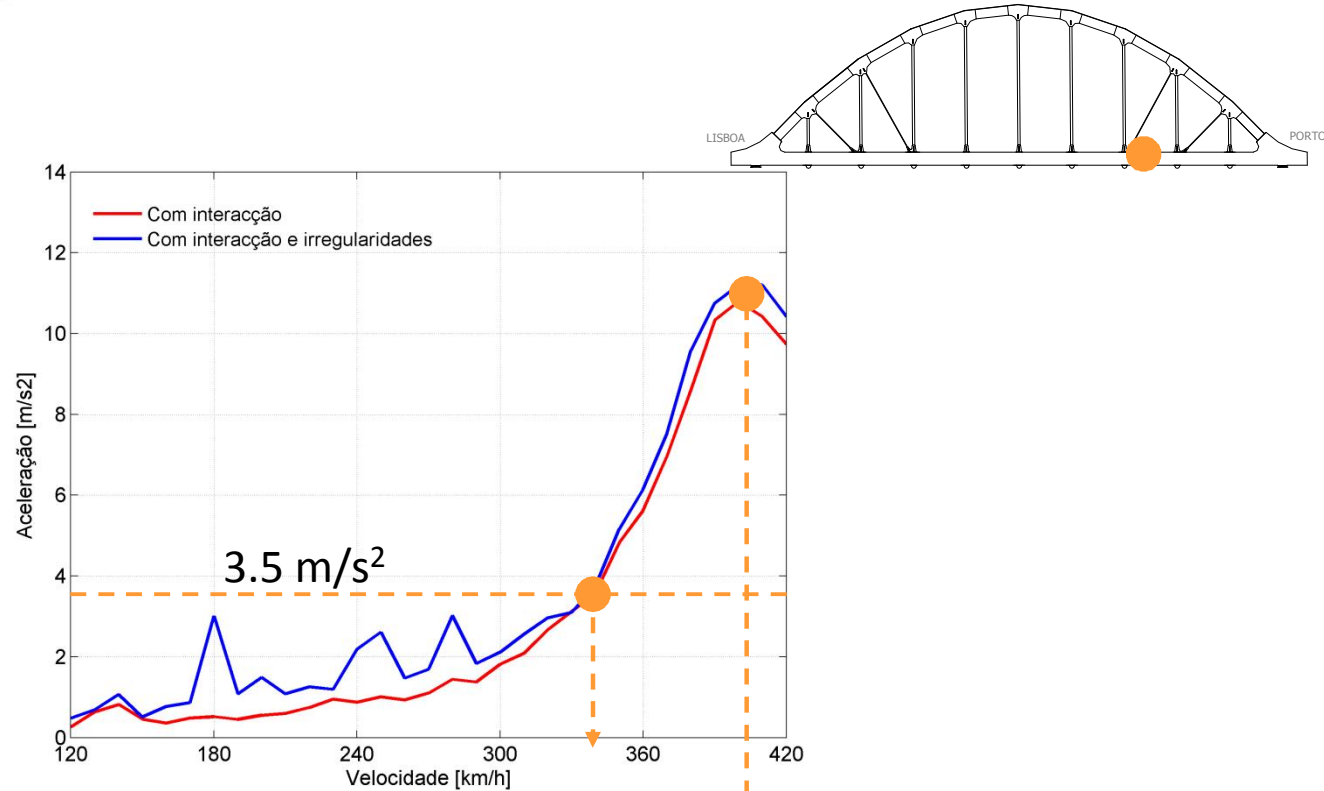


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Railway Stability



340 km/h

$$v_{res} \approx f_2 \cdot D \approx 4.38 \cdot 25.9 \approx 113.4 \text{ m/s} \approx 405 \text{ km/h}$$



Túlio N. Bittencourt  
 Universidade de São Paulo  
 São Paulo - Brazil



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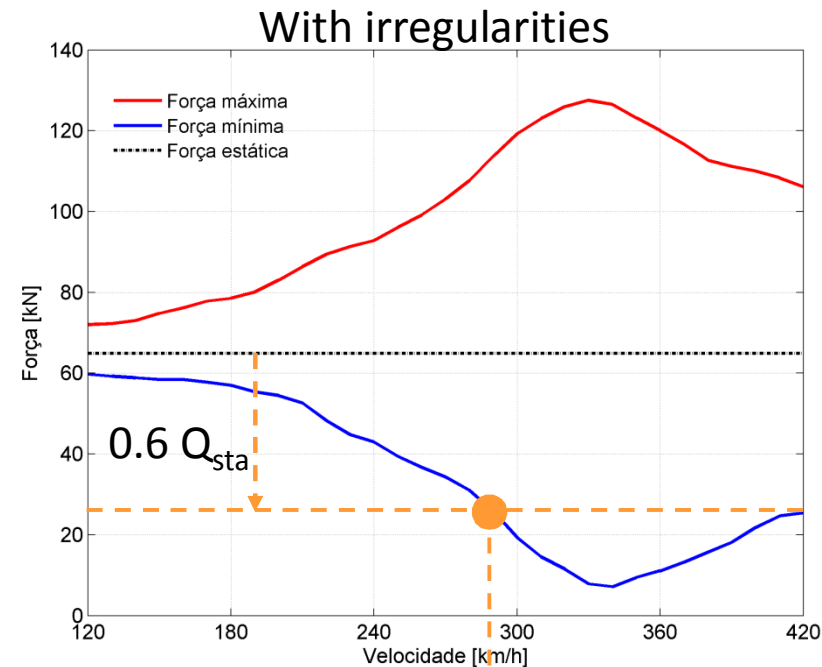
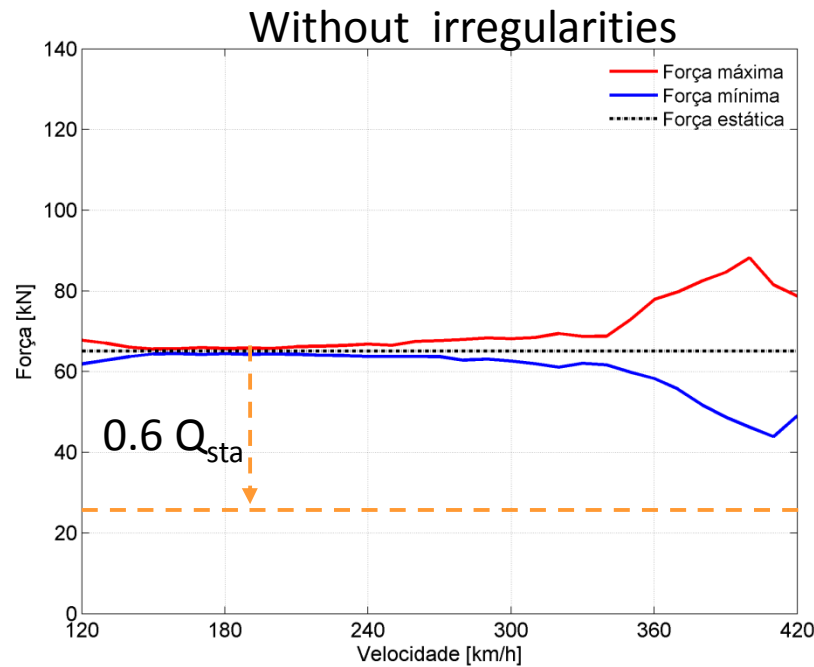
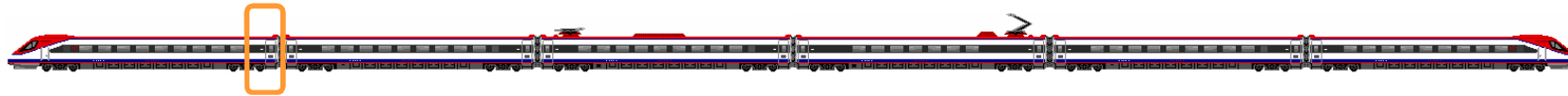


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## Stability of the contact between Wheel-Rail



285 km/h



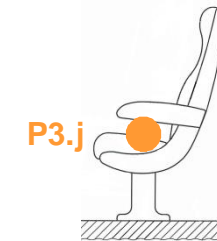
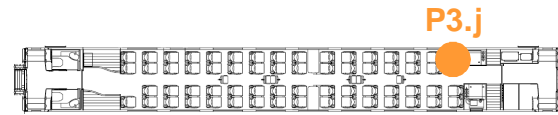


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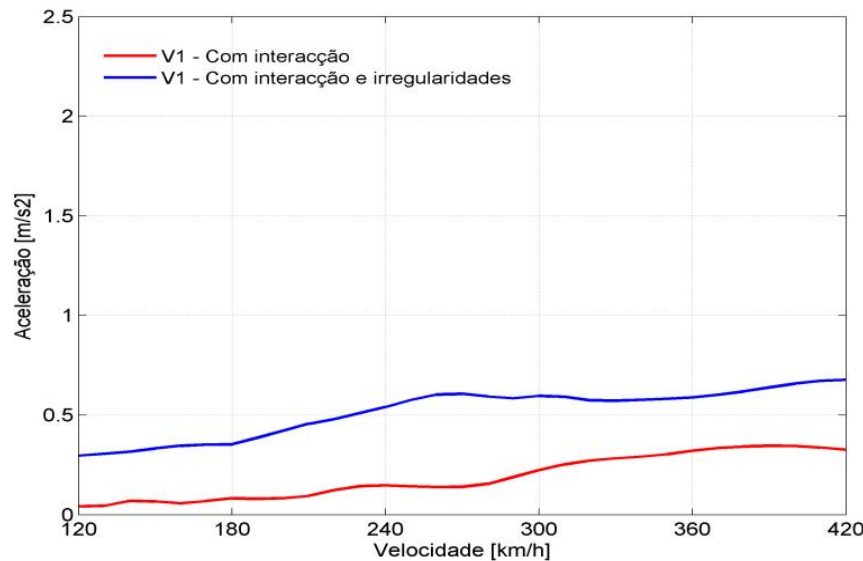
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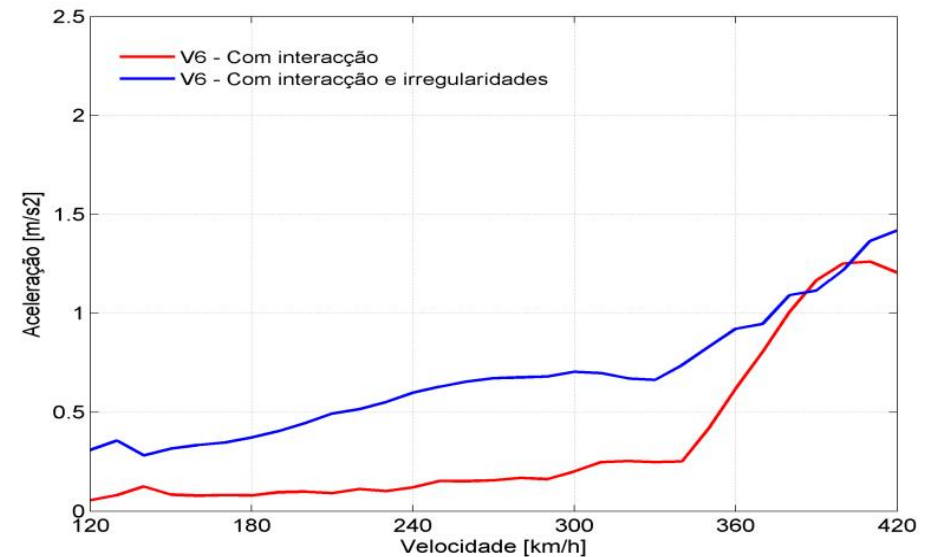
## Passengers Comfort



### Wagon 1



### Wagon 6



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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## Dynamic modeling of bridges in Portugal

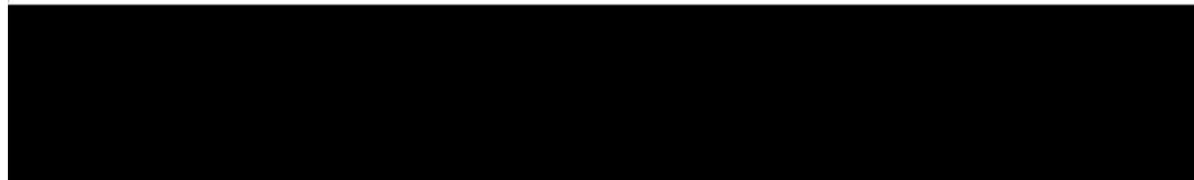
Courtesy: Prof. Rui Calçada - FEUP **U.**PORTO



Alcácer do Sal Bridge

(RIBEIRO, 2004)

Train-bridge  
interaction





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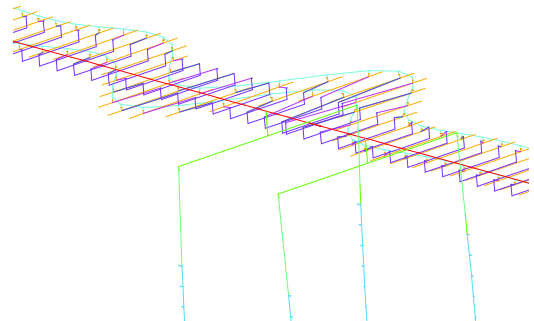
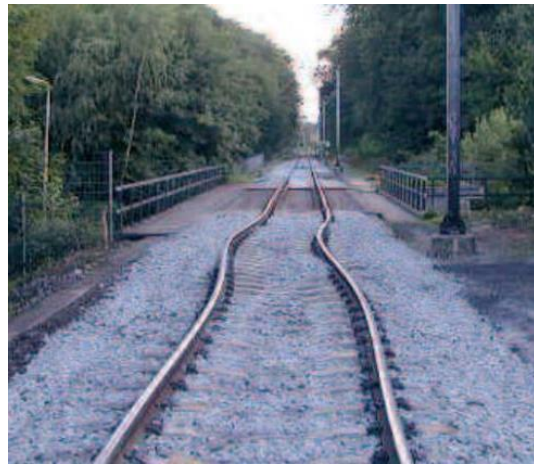
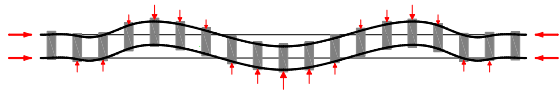


## Track-bridge interaction

Courtesy: Prof. Rui Calçada - FEUP

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## Conclusions

- ✓ The overview presented here shows the need to develop efficient modeling methodologies as supporting tools for the assessment of bridges;
- ✓ Technological developments in the rail transport sector has led to considerable requirements for the increase in the wagon load capacity (with associated heavy axle loads) and for high speeds (in the case of high speed railroads), posing new challenges in the field of structural evaluation of bridges;
- ✓ Advanced analysis techniques based on finite element methods have been successfully employed and are getting notorious development due to an increasing availability of computational resources, allowing a better level of model exploration;
- ✓ Such techniques should also have the ability to represent damage mechanisms and deterioration processes along time, such as fatigue damage and corrosion;



Túlio N. Bittencourt  
*Universidade de São Paulo*  
*São Paulo - Brazil*



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## Conclusions

- ✓ An efficient methodology is under development to enable a continuous integration between different analysis types, including static and dynamic procedures, necessary for fatigue assessment through iterative processes. Preliminary results have been shown here;
- ✓ FE models for fatigue assessment of steel railway bridges have been developed taking as a reference some existing bridges. The models are updated based on short-term monitoring and can present responses adjusted to the field measures;
- ✓ The dynamic behavior of bridges in high-speed lines is an important issue and has been briefly addressed, highlighting sophisticated tools of analysis that include track-bridge interaction and train-bridge interaction;



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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**Polytechnic School - University of São Paulo (USP) – Brazil**

<http://www.lmc.ep.usp.br/people/tbitten/gmec/home.htm>



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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**Obrigado pela sua atenção!**



Túlio N. Bittencourt  
Universidade de São Paulo  
São Paulo - Brazil



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